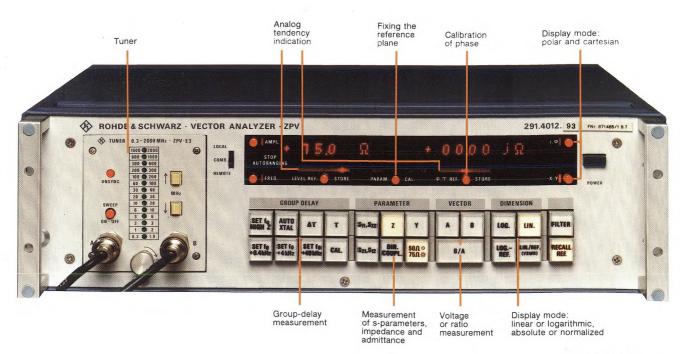
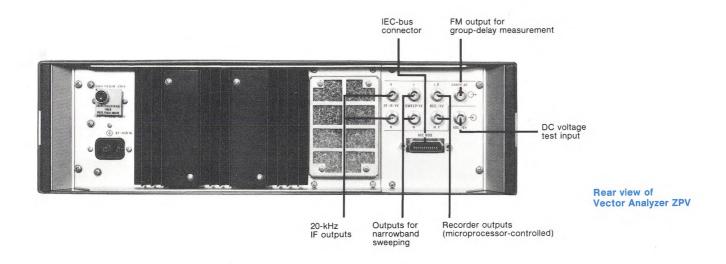


# VECTOR ANALYZER ZPV - Network analysis from 10 Hz to 2 GHz

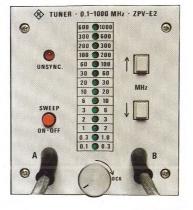


Front view of Vector Analyzer ZPV



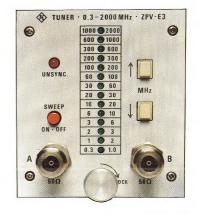


ZPV-E1



ZPV-E2

Tuners for ZPV



ZPV-E3

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### CODE NUMBER LIST

Code number list for Basic Software ZPV-K10 andS-parameter Accuracy-improvement Software ZPV-K1143

# CIRCUIT SYMBOLS

	Termination RNA or RNB (50 $\Omega$ , N male)
75 Ω	Termination (75 $\Omega$ )
	Short (50 Ω, N male)
<b>1</b> 75Ω	Short (75 Ω, N male)
Dez. B	Short (Dezifix B)
	Feed Unit ZPV-Z2 (50 $\Omega$ , 2 $ imes$ N female, 1 $ imes$ BNC female)
	Insertion Adapter ZPV-Z1 (50 $\Omega$ ) for channel A or B
	of the ZPV with Tuner ZPV-E2
10 dB	Attenuator DNF (50 Ω, 10 dB)
50/75Ω []-	Matching pad 50/75 $\Omega$
75/50Ω 	Matching pad 75/50 $\Omega$
	Directional Coupler ZPV-Z3 (50 $\Omega$ , RF input N male, others N female)
75,Ω	
	Directional Coupler ZWD-Z (75 $\Omega$ ); test item 75 $\Omega$ , Dezifix B
	others 50 $\Omega$ , Dezifix A
$\Diamond$	VSWR bridge (50 $\Omega$ ); e.g. ZRB 2
75 Ω	
$\diamond$	VSWR bridge (75 $\Omega$ ); e.g. SWOB4-Z
U	Coaxial angle (50 $\Omega$ , N male, N female)
	Coaxial tee (50 $\Omega$ , 2 × N female, 1 × N male)
75 Ω 	Coaxial tee (75 $\Omega$ )
A B	Pair of Test Cables ZPV-Z4 (50 $\Omega)$ for connection of channels A and B to Tuner ZPV-E3
$\times$	Test item
G ~	Signal generator
RAD	Feed-through termination RAD for adapting
	the ZPV-E1 to a 50- $\Omega$ system

.

## EQUIPMENT

### Brief description — Vector Analyzer ZPV

The functional principle of the Vector Analyzer ZPV is that of a **dual-channel vector voltmeter** measuring selectively magnitude and phase. The ZPV surpasses conventional vector voltmeters in operating and display convenience and nevertheless features an extremely favourable price/ performance ratio. The built-in microprocessor considerably simplifies complex measurement procedures converting the measured voltage into any parameter desired and displaying the result on the digital readout.

Different **tuner plug-ins** permit the ZPV to be matched to the required frequency range, thus enabling measurements in the AF range from 10 Hz right through to the analysis of subassemblies in the frequency range up to 2 GHz. The selective measuring method permits voltages down to 1  $\mu$ V to be measured. The dynamic range covers 120 dB. The external **signal generator** to be connected is selected in accordance with the requirements of the specific measurement task. Whereas a high-precision synthesizer is required for determining the data of a crystal or a crystal filter, the generator used for measuring wideband filters need not have such outstanding capabilities.

All the functions of the ZPV are **programmable**, i. e. the IEC-bus sets all operating modes and outputs all test results. The minimum time required for one measurement of amplitude **and** phase is 35 ms. The S-parameter Test Adapter ZPV-Z5 permits automatic measurements of all four s parameters without modification to the test setup.

Vector Analyzer ZPV is described in detail in Data Sheet 292401.

### Basic unit



The basic unit, a 20-kHz selective two-channel receiver, processes the input signals converted by the tuner to an IF

of 20 kHz. The built-in microprocessor handles all the control, input and output functions plus error correction as well as the conversion of the measured voltages into any parameter required. Thanks to different tuner plug-ins and accessories (directional coupler, VSWR bridges, etc.), the basic unit can be fitted to meet the user's requirements regarding frequency range and measuring method.

#### Tuner ZPV-E1



**Frequency range** The Tuner ZPV-E1 covers the frequency range from 10 Hz to 50 MHz and tunes automatically to the frequency of the signal applied to the synchronization input. Depending on the frequency and amplitude of the input voltage, it selects a bandwidth of 10 Hz, 200 Hz or 1 kHz. This autoranging facility can be disabled via the IEC

bus; the bandwidth can then be programmed by the user as required.

**Inputs** High-impedance inputs (1 M $\Omega$  shunted by 17 pF) are used throughout; they are fitted with BNC female connectors permitting the use of conventional probes or 10:1 attenuator probes. With the U × 10 buttons pressed, the basic unit takes into account the division factor of 10. Insertion adapters enable measurements in systems using 50  $\Omega$  coax.

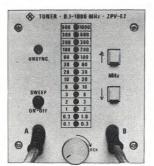
The highest permissible input voltage is 1 V, 10 V with a 10:1 attenuator probe. Due to the low inherent noise of 3  $\mu$ V (typ. 1  $\mu$ V), reproducible measurements can be made even with low-level signals driving the item under test.

**Measurement capabilities** The ZPV-E1 permits impedances, admittances, s parameters, reflection coefficients, etc. to be determined. Its lower limit frequency of 10 Hz enables the measurement of the amplitude and phase response of control loops. The direct display of the amplitude and phase on the basic unit facilitates the evaluation of stability criteria.

With the built-in frequency counter, group-delay measurements are possible not only with the frequency deviations preset on the basic unit (0.4/4/40 kHz) but with any other deviation desired. The microprocessor calculates the group delay from two phase and two frequency values and reads the result out on the display.

**Description** The ZPV-E1 for the Vector Analyzer ZPV is a two-channel heterodyne receiver which selectively measures the amplitude and phase of the signals present at the two inputs A and B. The selective measurement method makes the ZPV-E1 largely insensitive to the harmonics of the voltage to be measured and to other interfering signals which might cause considerable measurement errors when using wideband phase meters.

### Tuner ZPV-E2



Frequency range The Tuner ZPV-E2 covers the frequency range from 100 kHz to 1 GHz (typ. 1.2 GHz) in 14 subranges. The measurement is made selectively depending on the amplitude of the voltage to be measured at a bandwidth of 30 Hz or 2 kHz.

**Inputs** Its two associated probes permit voltages to be measured with high impedance. Insertion units can be combined with the probes for measurements in coaxial systems. Directional couplers can also be connected via the insertion units.

Measurement capabilities In general, all the measurements that the many measuring and processing capabilities of the basic unit offers can be made with the ZPV-E2. Below 100 MHz, reflection measurements are possible without directional couplers or VSWR bridges. The microprocessor included in the basic unit converts the result accordingly.

Due to its high measuring accuracy and favourable frequency range, the ZPV-E2 is ideal for crystal measurements. Crystal equivalent-circuit parameters can be determined within a few seconds.

**Description** The Tuner converts the input signals of the channels A and B with the aid of two sampling mixer stages to the IF of 20 kHz, the fundamental of the input signals being retained with amplitude and phase fidelity. To a certain degree, the curve shape is also maintained if the spectral components do not considerably exceed 1 GHz (2 GHz with Tuner ZPV-E3).

Within a frequency subrange, tuning to the fundamental of the input signal of channel A is automatically performed by the frequency control circuit and a VCO. Channel B is then tuned to the same input frequency. The subrange is selected either by way of the switch-selected autoranging facility on the basic unit or manually on the front panel of the Tuner.

### Tuner ZPV-E3



Frequency range The frequency range of the Tuner ZPV-E3 covering 300 kHz to 2000 MHz is twice that of the Tuner with probes, ZPV-E2. This considerably extends the application range of the basic unit. The ZPV-E3 permits vector two-port and group-delay measurements in **coaxial** systems over a wide frequency and level range. Depend-

ing on the amplitude of the voltage to be measured, selective measurements at a bandwidth of 30 Hz or 2 kHz are possible.

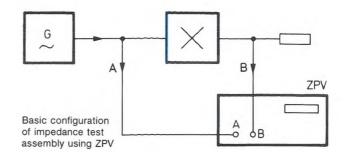
**Inputs** The impedance of the test inputs fitted with N female connectors is  $50 \Omega$ . This permits **simple and straightforward test assemblies** to be set up since the test circuits used can be connected directly to the ZPV-E3. There is no need for the insertion unit and the associated termination required with the ZPV-E2. Measurement capabilities In conjunction with the Tuner ZPV-E3, it is possible to take full advantage of the measuring and processing capabilities offered by the basic unit. Reflection-coefficient and impedance measurements can be made with **directional couplers** or **VSWR bridges** or by the simple **T-junction method**. The latter is an entirely new measuring method that greatly simplifies the test setup and, as a result, drastically cuts down its costs. After entry of the type of desired test setup at the push of a button on the basic unit, the parameter of interest is calculated by the microprocessor and read out digitally. Whereas the entire frequency range of the Tuner ZPV-E3 can be utilized with the T-junction method, directional couplers or VSWR bridges restrict the frequency range according to their particular characteristics.

Description Same as for Tuner ZPV-E2.

## EQUIPMENT

### Signal generators extend ZPV to test assembly

A range of manual and programmable signal generators is available from Rohde & Schwarz to extend the ZPV to a complete impedance test assembly. The following table lists the most important generators in the AF range (SPN, SMK) up to and beyond 2 GHz (SWP).



### Generators

Frequency range	Designation	Туре	Order No.	Frequency error	Frequency resolution/ indication	Output level EMF
1 Hz to 1.3 MHz	Generator	SPN	336.3019.02	$1 \times 10^{-5}$ /month 1 × 10^{-6}/°C	0.1 Hz. 4-digit display	Sin.: 1 mV to 10 V Square: TTL level $Z_o: 600/50/ \approx 5 \Omega$
10 Hz to 140 MHz	Signal Generator	SMK	348.0010.02	(crystal; synthesizer)	1 Hz, 9-digit display	$0.025~\mu V$ to 2 V into 50 $\Omega$ ( $-138.9$ to $+19~dBm)$
0.1 to 1040 MHz	Signal Generator	SMS 2	372.2019.28	(crystal; synthesizer)	100 Hz, 8-digit display	0.03 $\mu V$ to 1 V into 50 $\Omega$ (–137 to +13 dBm)
5 kHz to 1360 MHz	Signal Generator	SMPC	300.1000.52	(crystal; synthesizer, 1 × 10 <sup>-8</sup> /day)	0.1 Hz, 10-digit display	0.016 $\mu V$ to 1 V into 50 $\Omega$ (-143 to +13 dBm)
5 kHz to 1360 MHz	Synthesizer Generator	XPC	337.8014.52	(crystal; synthesizer, 10 MHz; 1 × 10 <sup>-8</sup> /day)	0.1 Hz 10-digit display	0.016 $\mu V$ to 1 V into 50 $\Omega$ (–143 to +13 dBm)
0.1 to 2500 MHz	Sweep Generator	SWP	339.0010.02	(crystal)	1 kHz, 6-digit display	0.7 μV to 707 mV (-110 to +10 dBm)
5 kHz to 2720 MHz	Signal Generator	SMPD	376.8011.52	(crystal; synthesizer, 2 × 10 <sup>-9</sup> /day)	0.1 Hz up to 1000 MHz, 1 Hz beyond 1000 MHz, 10-digit display	0.016 μV to 1 V into 50 Ω (-143 to +13 dBm)

### S-parameter Test Adapter ZPV-Z5 • 5 to 2500 MHz

In conjunction with a suitable network analyzer, e.g. the Vector Analyzer ZPV, the S-parameter Test Adapter ZPV-Z5 permits measurement of all four s parameters without modification to the test setup.

#### Characteristics and uses

**High directivity, wide frequency range** Thanks to the high directivity of the VSWR bridges of 46 dB, even items with very small reflection coefficients can be tested. The Test Adapter covers almost the entire frequency range of the Tuner ZPV-E3 due to its wide bandwidth of 5 to 2500 MHz; it can of course also be used with the Tuner ZPV-E2 in the range 5 to 1000 MHz.

**IEC-bus compatibility** The Test Adapter can be controlled via the IEC bus and thus combined with an IEC-buscompatible signal generator and a desktop computer to form an attractively priced, automatic network analyzer.

**Connections, settings, measurements** The Test Adapter is connected to the RF generator and to channels A and B of the Vector Analyzer (see page 26). The test item input and output are taken to ports 1 and 2 of the ZPV-Z5.

In manual operation the s parameter to be measured is selected by pressing the corresponding front-panel key; in automatic operation it is set via the IEC bus by a desktop computer, e. g. the Process Controller PUC.

The key labelling and the programming commands correspond to the s parameters to be measured. To measure for instance the input reflection coefficient  $s_{11}$ , S11 is simply entered via the computer.

#### Description

The ZPV-Z5 is of symmetrical design to permit the measurement of input and output parameters. The reference branch includes a line for compensating the electrical lengths in the test branches; tedious length compensation by adding a suitable line section is thus no longer required. If a test item cannot be linked up directly to the test sockets of the ZPV-Z5, the input and output of the test item need simply be connected via identical cable sections and a third section of the same length inserted into the reference branch. To provide a power supply for active components, two DC Feed Units ZPV-Z6 can be connected.

## EQUIPMENT



### When combining the Vector Analyzer ZPV with an IEC-buscompatible generator and a control computer, an automatic network analyzer system is obtained for use over the frequency range from 10 Hz to 2 GHz.

Basically any IEC-bus-compatible generator can be used. For applications where a frequency resolution of 100 Hz is sufficient, Rohde & Schwarz offers the Signal Generator SMS 2 (0.1 to 1040 MHz). To measure extremely narrowband test items, such as crystals or crystal filters, the Synthesizer Generator SMPC (0.05 to 1360 MHz) is recommended permitting frequency variation in 0.1-Hz steps below 100 MHz.

IEC-bus-compatible control computers fitted with a screen enable the measured values to be plotted in diagrams. For this purpose, Rohde & Schwarz offers the Process Controller PUC.

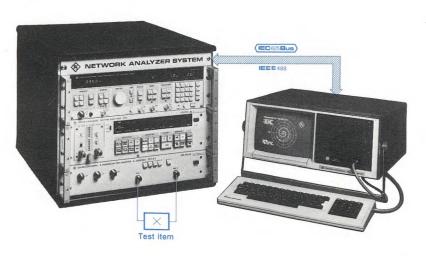
With the easy-to-handle **Basic Software** available for the network analyzer system based on the ZPV, a minimum of time is required to get acquainted with the use of the system. To ensure increased accuracy, the **S-parameter Ac-curacy Improvement Software** is available permitting for instance errors introduced by the test setup to be eliminated. The preprogrammed measurement and display modes can be called up with code numbers (see page 43). Graphic display in particular shows the efficiency of the software: the plotted diagrams can be made available as hard-copy documentation. Data sheet 292211 gives a detailed description of the software for the ZPV.

**All** the s parameters of a test item can be measured with the S-parameter Test Adapter ZPV-Z5 (see data sheet 335111) without modification to the test setup.

## = automatic network analyzer system

The resulting network analyzer system is easy to program, features a high test speed and involves low costs; it permits all the measurements possible with the ZPV to be performed automatically.

Automatic network analyzer system for 5 MHz to 2 GHz, comprising Vector Analyzer ZPV, Sweep Generator SWP, S-parameter Test Adapter ZPV-Z5 and Process Controller PUC

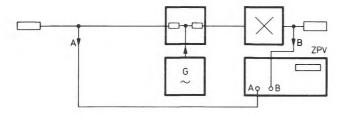


### Example 1

Determining the compression of a 10-dB amplifier at 10  $\mbox{MHz}$ 

### Test setup and principle

Transmission measurement



### **Test procedure**

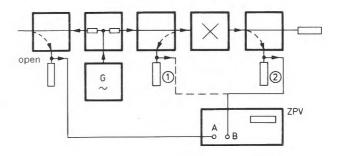
Set the RF level at the signal generator so that the amplifier operates in its linear range. Measure gain B/A and store as reference value. Increase RF level until B/A reaches a value of, say, -1 dB. Now measure voltage in channel A.

### Example 2

Measuring the four s parameters of a transistor

#### Test setup and principle

Transmission and reflection measurement

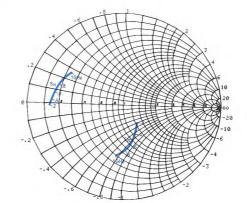


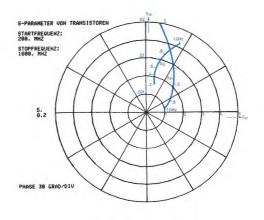
#### **Test procedure**

Connect channel B of ZPV depending on s parameter to be measured: directional coupler (1) for  $s_{11}$ ,  $s_{22}$ ; directional coupler (2) for  $s_{21}$ ,  $s_{12}$ . Results can be read off directly as a function of frequency or traced with an XY recorder.

The measurement setup and procedure can be considerably simplified and, particularly in computer-controlled operation, accelerated, by the use of the S-parameter Test Adapter ZPV-Z5 (page 8). Power for the active circuit elements is provided by the DC power supply ZPV-Z6 (shown on page 41).

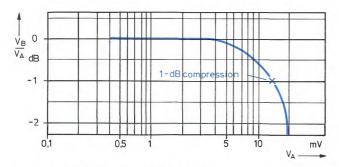
### **Test result**





#### Test result

V <sub>A</sub> [mV]	0.4	0.6	0.8	1.04	5	
V <sub>B</sub> /V <sub>A</sub> [dB]	0	0	0	0	-0.04	
V <sub>A</sub> [mV]	10.4	11.6	13.1	14.7	20.8	
V <sub>B</sub> /V <sub>A</sub> [dB]	-0.48	-0.57	-0.78	-1	-2.1	



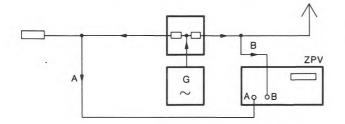
Compression of a 10-dB amplifier at 10 MHz

### Example 3

Antenna matching

#### Test setup and principle

Reflection measurement with 3-point correction



#### **Measurement procedure**

For the possibility that a large antenna mismatch may exist (antenna output impedance 1  $\Omega$  to >1 k\Omega), use of the s-parameter (3-point) correction software is advisable. An additional advantage is that the effect of the (possibly long) antenna lead may be eliminated by means of short-circuit, zero-load and 50- $\Omega$  calibration at the antenna base.

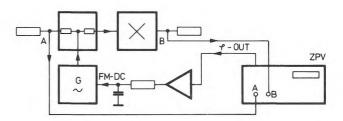
The digital indication of the ZPV is particularly convenient for measurement in antenna fields when phase differences between individual elements are to be determined.



Determining the series-resonance frequency of crystals

#### Test setup and principle

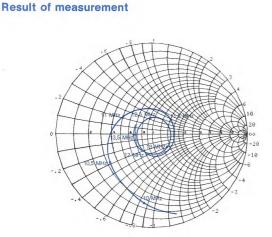
Transmission measurement



#### **Test procedure**

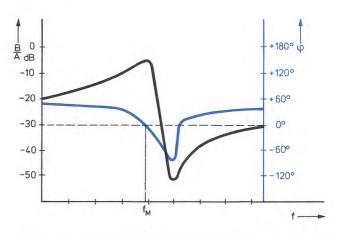
Change the signal-generator frequency manually until the voltage ratio B/A reaches a maximum using the quasianalog tendency indication of the ZPV as an aid. The feedback loop then pulls the generator to the series-resonance frequency. Select the resolution of the counter to permit the frequency to be read to within 1 or 0.1 Hz.

An alternative is offered by the computer program "Digital Control Loop". It determines with a mathematical iteration procedure the frequencies at which the phase is  $0^{\circ}$  and  $\pm 45^{\circ}$ , and from this the Q and equivalent-circuit values of the crystal. The measurement requires about 10 seconds.



Impedance of a log-periodic broadband antenna as a function of the frequency

#### Test result



Phase (blue) and amplitude of the crystal response as a function of frequency

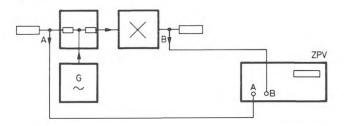
**Note:** The design of the crystal adapter is specified in the German standard DIN 45105.

### Example 5

Checking the accuracy of a step attenuator

#### Test setup and principle

Transmission measurement



#### **Test procedure**

Set the step attenuator initially to 0 dB. Measure value of  $V_{\rm B}/V_{\rm A}$  and store as reference in dB.

Then change attenuation in steps as required, noting the measured value. High accuracy is attainable, since the error of the ZPV is less than  $\pm 1.5\%$  (equivalent to 0.13 dB).

#### **Test result**

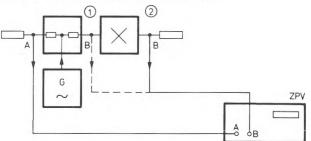
Nominal value (dB)	Measured value (dB)
40	39.7
50	50.5
60	60.4
70	69.5

Example 6

Measuring the amplitude/frequency response characteristic of a broadband amplifier, frequency range 5 to 500 MHz, gain 10 dB. Examination of the s parameters of the amplifier.

#### Test setup and principle

Transmission and reflection measurement

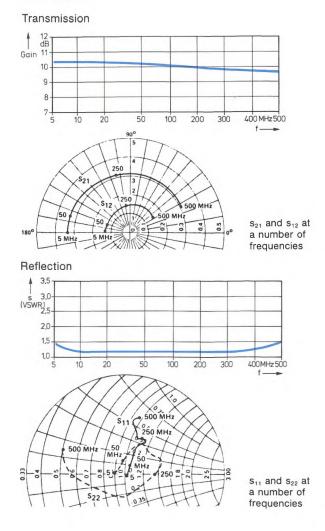


### Test procedure

Tune the frequency of the signal generator through the range of interest. Measure voltage ratio B/A either as absolute value or in relation to any reference value. The measurement of the ratio makes the result independent of variations in the output level of the generator.

Transmission measurement: probe B at output, point (2) Reflection measurement: probe B at input, point (1)

#### **Test result**



12

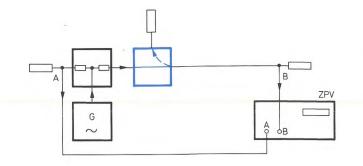
### Example 7

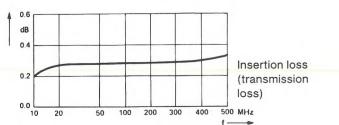
Measuring the principal parameters of directional couplers (see also page 39) including documentation of results for final production testing. 20-dB directional coupler (shown blue) for frequency range 10 to 500 MHz.

#### **Test setup**

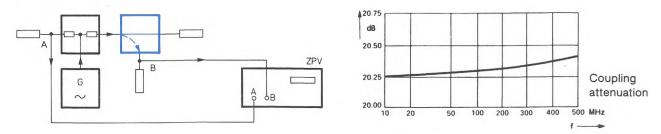
**Test result** 

Insertion loss (transmission loss)

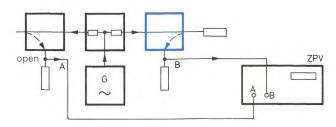


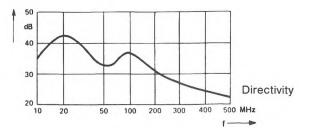


Coupling attenuation

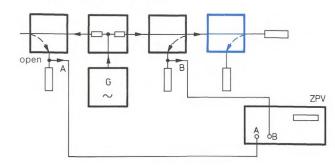


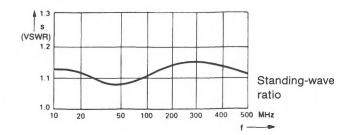
Directivity





Standing-wave ratio (VSWR)



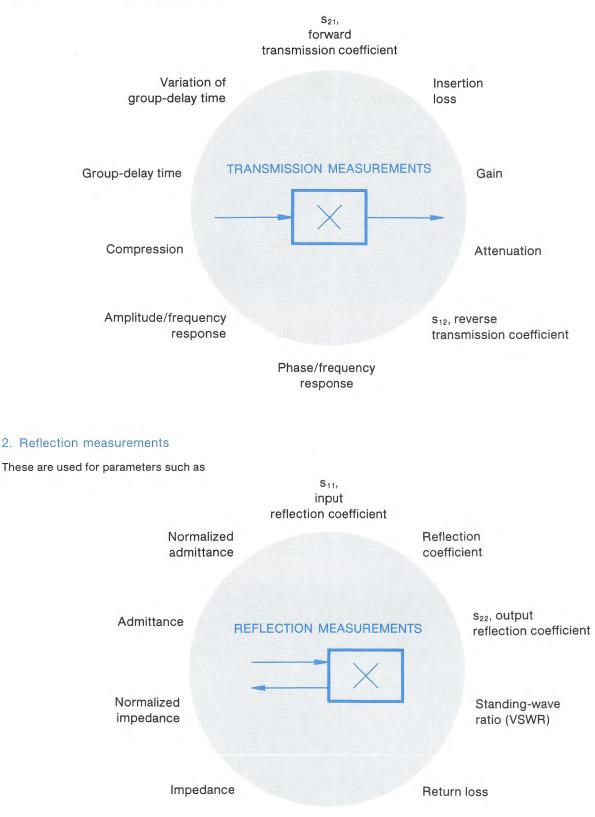


### Summary

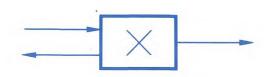
Before each measurement it must be decided which parameters are to be found. This then determines the test setup to be used. Three distinct cases can be identified:

### 1. Transmission measurements

These are used for parameters such as



### 3. Reflection and transmission measurements

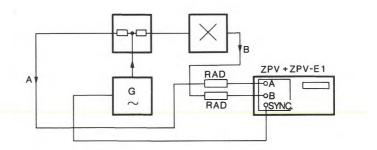


# Choosing the correct measurement and calibration setups

The tables which follow have been arranged in accordance with these three different cases. The various frequency ranges are also given and a distinction made between setups which are suitable for  $50-\Omega$  or  $75-\Omega$  systems. Since the Vector Analyzer ZPV is a  $50-\Omega$  instrument, matching pads will be needed for measurements in  $75-\Omega$  systems. The connectors necessary at the test object are also shown for each setup so that there will be no need to add extra adapters.

This information is not given when the test item is to be connected to components not supplied by Rohde & Schwarz, in such cases a number of different connectors may be used.

**Note:** In using the ZPV with Tuner ZPV-E1 in a 50- $\Omega$  system, the inputs of the tuner must each be provided with a feed-through termination RAD (order number 289.8966.00). The RADs (50  $\Omega$  between inner conductor and ground) prevent falsification of the measurements by reflections that could result because of a mismatch with the high-resistance tuner inputs. Furthermore, the generator signal, either of sinewave or rectangular form, must be supplied to the SYNC input of the tuner at a level of at least 20 mV (10 mV for f > 25 kHz).



Test setup for transmission measurements with Tuner ZPV-E1, the inputting into ZPV-Z2 with two N-to-BNC transitions, as well as two feed-through terminations RAD at the tuner inputs

For achieving the highest measurement accuracy at frequencies above 100 MHz by use of Tuner ZPV-E2, 10-dB attenuation elements in front of the transmission adapter are recommended. The self-reflection factor is then negligibly small.

Order designations and numbers are tabulated on pages 32 to 37.

#### The choice of the required measurement or calibration setup is made in the following steps:

- 1. Which of the above three cases is involved?
- 2. Is the impedance of the connectors on the test item 50  $\Omega$  or 75  $\Omega$ ?
- 3. What is the frequency range of interest?

#### Answer

Case 1, 2 or 3

50  $\Omega$ : lefthand half of following pages 75  $\Omega$ : righthand half of following pages

ro az. righthand han or following paged

Measurement may/must use

- neither directional couplers nor VSWR bridge
- directional couplers
- VSWR bridge
- and requires the following instruments
- ZPV with Tuner ZPV-E1
- ZPV with Tuner ZPV-E2 or
- ZPV with Tuner ZPV-E3



X

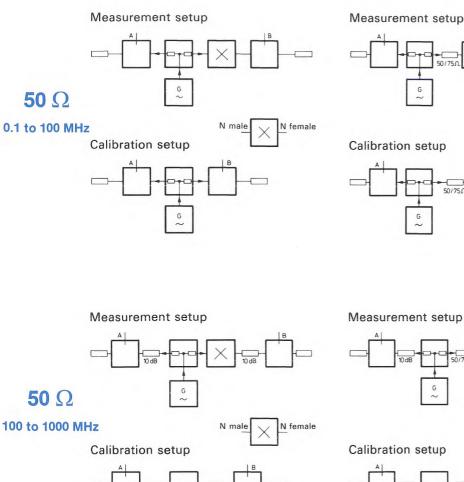
50/75

50/75 D

G

G 2

### Using Vector Analyzer ZPV with Tuner ZPV-E2 (0.1 to 1000 MHz)



G

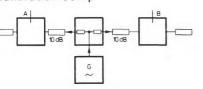
75/50A

**75**Ω

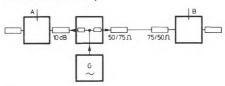
**75**Ω

0.1 to 100 MHz

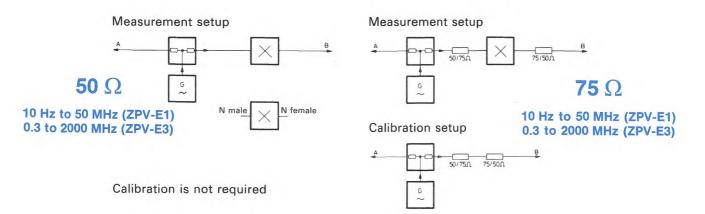
100 to 1000 MHz







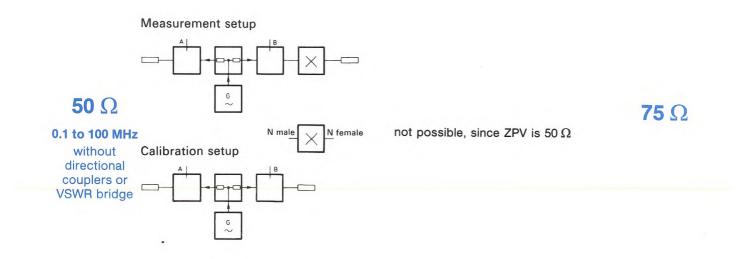
Using Vector Analyzer ZPV with Tuner ZPV-E3 (0.3 to 2000 MHz) or Tuner ZPV-E1 (10 Hz to 50 MHz) with use of RADs (page 15)

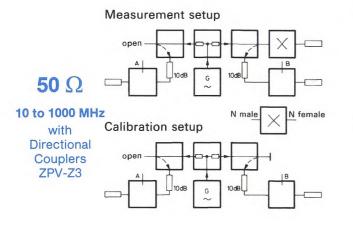


Reflection measurements

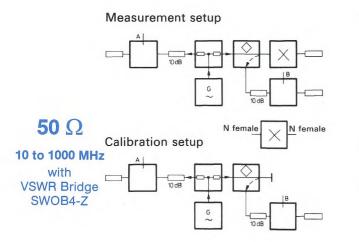
 $\rightarrow \times$ 

Using Vector Analyzer ZPV with Tuner ZPV-E2 (0.1 to 1000 MHz)

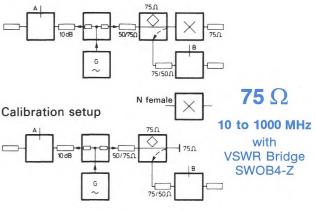




Measurement setup 75 N 75 N 75<u>Л</u> oper **75**Ω G 10 to 1000 MHz Dez. B X Calibration setup with Directional 75 N Couplers open Dez. B ZWD-Z G



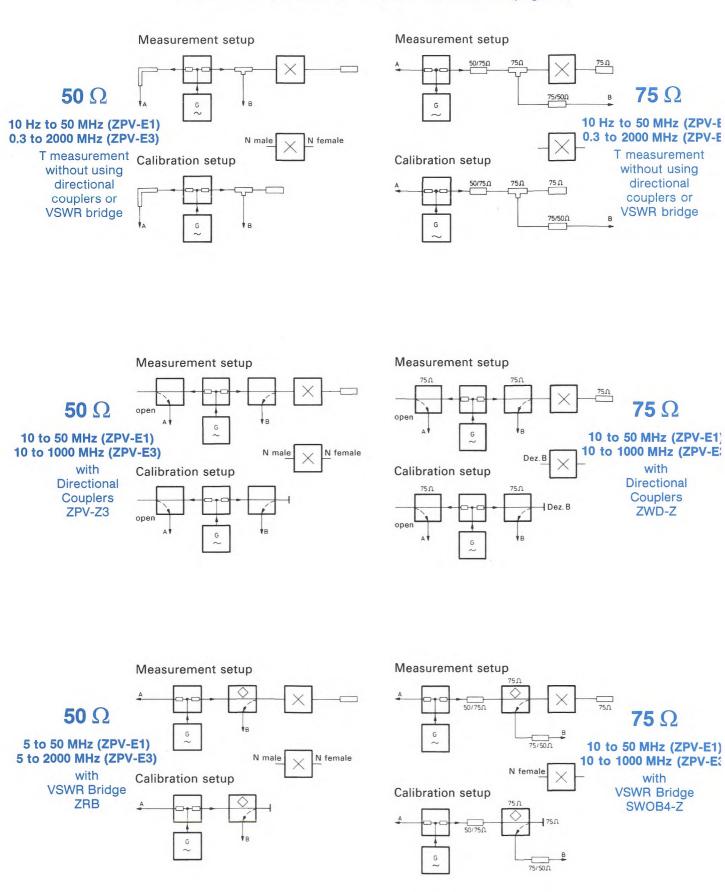
Measurement setup





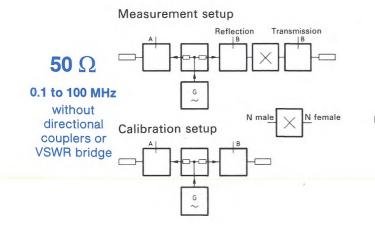
s 🚞 🗙

Using Vector Analyzer ZPV with Tuner ZPV-E3 (0.3 to 2000 MHz) or Tuner ZPV-E1 (10 Hz to 50 MHz) with use of RADs (page 15)

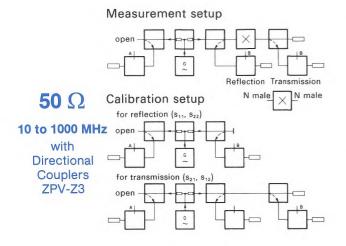


Reflection and transmission measurements

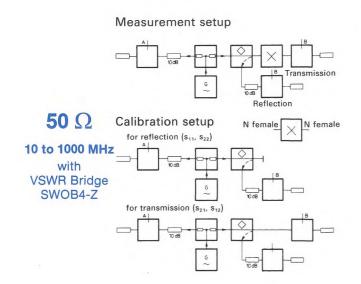
Using Vector Analyzer ZPV with Tuner ZPV-E2 (0.1 to 1000 MHz)



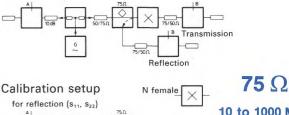
not possible, since ZPV is 50  $\Omega$ 



#### Measurement setup open G Reflection Transmission Calibration setup **75**Ω Dez. B Dez. B for reflection (s11, S22) 10 to 1000 MHz oper H Dez. B with G Directional for transmission (s21, s12) Couplers ZWD-Z open G



Measurement setup



50/750

G

G

for transmission (s21, S12)

1750

5/500

75/500



**75**Ω

SWOB4-Z

Reflection and transmission measurements



Using Vector Analyzer ZPV with Tuner ZPV-E3 (0.3 to 2000 MHz) or Tuner ZPV-E1 (10 Hz to 50 MHz) with use of RADs (page 15)

## **50** Q

### 10 Hz to 50 MHz (ZPV-E1) 0.3 to 2000 MHz (ZPV-E3)

T measurement without using directional couplers or **VSWR** bridge

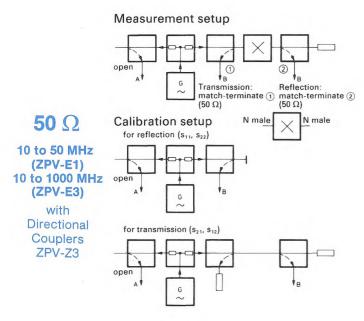
Combined measurement setup is not possible; refer to setups given for "Transmission measurements" and "Reflection measurements".

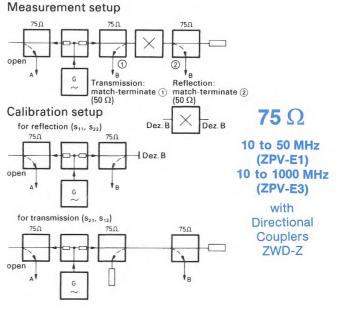
Combined measurement setup is not possible; refer to setups given for "Transmission measurements" and "Reflection measurements".

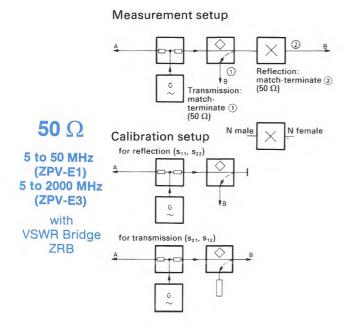


### 10 Hz to 50 MHz (ZPV-E1) 0.3 to 2000 MHz (ZPV-E3)

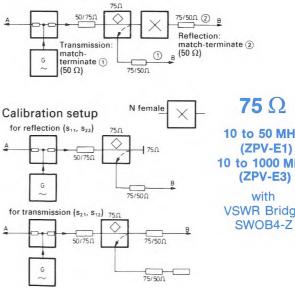
T measurement without using directional couplers or VSWR bridge







Measurement setup



## **75** $\Omega$



The purpose of this section is to demonstrate which combination of keys is required for measuring any required parameter. All keys which are not referred to are switched off. The measurement setup should be selected from those given in the preceding section. Only the special case of group-delay measurement is described separately in this section.

### Voltage measurement

#### Storing a reference value

The ZPV measures voltage vectors according to both amplitude and phase. The measurement can be made either in absolute terms or with reference to any desired value.

The reference value is stored using the following buttons on the display panel:

LEVEL REF. O STORE	Amplitude
P, T REF. O STORE	Phase
PARAM. O CAL.	Amplitude and phase

Different values may be stored for channel A, channel B and for the ratio  $\mathsf{B}/\mathsf{A}.$ 

#### Storage procedure

- Press the required combination of keys (see table on page 22; absolute values only)
- Set reference value
- Store reference value (see above)

Check: press REF. and observe that the stored value

appears on the display

Press RECALL again to release

Key combinations: see table on page 22

#### Measurement procedure

- Fix reference value if required
- Press appropriate key combination
- Set test frequency on signal generator —
- Read out measurement result

#### Example

The insertion loss of a filter at the centre frequency  $f_c$  is 5.6 dB. It is required to find the two cutoff frequencies at which the attenuation has increased by 6 dB.

#### Procedure

- Set signal generator to f<sub>c</sub>
- Press
   B / A
   Luce. on the ZPV
   (display reads 5.6 dB)
- Press PARAM. 
   CAL. (Check by pressing 
   REF.
   Again to release.)
   REF.
   A Press
   Action
   Action
- Press LOG.-REF. (display reads 0 dB)
- Vary signal-generator frequency upwards and downwards until display reads –6 dB
- Read the cutoff frequencies at the signal generator

### S-parameter measurement

The parameters covered in this section are:  $s_{11}$ ,  $s_{22}$ ,  $s_{21}$ ,  $s_{12}$ , Z, Y, Z/Z<sub>o</sub>, Y/Y<sub>o</sub>, VSWR, return loss and insertion loss (see summary of reflection and transmission measurements on page 14).

Before an s-parameter measurement is made, the reference plane must be established. The calibration setup required is to be found in the previous section "Measurement and calibration setups". Recalibration will only be required if the measurement setup is changed, e.g. when going from a  $50-\Omega$  to a  $75-\Omega$  setup.

#### Establishing the reference plane

- Assemble the correct calibration setup
- On the ZPV press st1, 522 or s12, 512 Z Y
   and LIK.
- Depending on the calibration setup bill, coupl. and/or should also be pressed

Regarding high-impedance measurements (HIGH-Z method), see page 39.

#### For a reflection measurement



#### For a reflection/transmission measurement

•	Press	\$ <sub>21,</sub> \$ <sub>12</sub>	LIN.	PARAM. 🔵 CAL.	to fix reference plane
---	-------	------------------------------------	------	---------------	------------------------

**Note:** Compensation for attenuation pads in the circuit takes place automatically since they are accounted for in the calibration routine.

Key combinations: see table on page 23

#### Measurement procedure

- Calibrate measurement setup (see section "Measurement and calibration setups")
- Press required key combination
- Set test frequency on signal generator —
- Read off measurement result \_\_\_\_\_

**Note:** When the S-parameter Test Adapter ZPV-Z5 is used, the key for the desired s parameter must also be pressed (e. g.  $S_{11}$ ).

## Table of key combinations for voltage measurements

	Key combination	Display mode and dimension	Examples of display
Voltage			
	ЦИ., ε, φ   🜑	linear in mV, amplitude and phase	100 mV +135 φBA
Absolute values		logorithmic in dDm	
	LOG. 1, 9 🖡 🔘	logarithmic in dBm, amplitude and phase	<b>−6.9 dBm +135</b> <i>φ</i> <b>BA</b>
in channel A or B			
Relative to any reference value	LIN, / REF. (V/S/WR) r, Y	linear, amplitude and phase	2 0.0 φΒΑ
	LOGREF. 7, 9 ]	logarithmic in dB, amplitude and phase	+6. dΒ 0.0 φΒΑ
Voltage ratio	_		
	LIN. r, 4 i 💿 Or	linear, amplitude and phase	.016 –31.0 φ <b>BA</b>
	X,Y   🔘	or real and imaginary parts	+.014 –.0087 j
Absolute values			
	L0G. r, 4	logarithmic in dB, amplitude and phase	–35.6 dB –31.0 φBA
В/А			
		linear, amplitude and phase	.500 –175. φ <b>BA</b>
Relative to any	X,Y   ●	or real and imaginary parts	497042 j
reference value	LOGREF. r, 9	logarithmic in dB, amplitude and phase	–6.0 dB –175.1 φBA

### Table of key combinations for s-parameter measurements

	Basic settings for measurements without directional couplers or VSWR bridge and <b>50-<math>\Omega</math> test item</b>	Also required with <b>75-</b> Ω <b>test item</b>	Also required when using direc- tional couplers or VSWR bridge
Transmission measurements			
Forward transmission coefficient s <sub>21</sub>	s <sub>21,</sub> s <sub>12</sub> LIK. r, φ <b>i</b> • Or X, Y <b>i</b> •	50 A ~ 75 A *	DIR. COUPL.
Insertion loss (transmission loss)	S <sub>21,</sub> S <sub>12</sub> [LOG. r, <i>φ</i> ] ●	50 Å ° 75 Å *	DIR. COUPL.
Reverse transmission coefficient s <sub>12</sub>	S <sub>21,512</sub> LIN. r, 𝒫 I ● OT X, Y I ●	50 Å ° 75 Å *	DIR. COUPL.
<b>Special case:</b> High impedances (see page 39)	2 Ι.Ι	50 Å ° 75 Å • NIGH-2	—
Very low admittances (see page 39)	Υ LIR. e, φ [ • Or X, Y ] •	50 Д ° 75 Д • НСН-2	—
Reflection measurements			
Input reflection coefficient s11	S <sub>111</sub> , S <sub>22</sub> Lin. r, φ <b>i</b> • Or X, Y <b>i</b> •	50 A ° 75 A •	DIR. COUPL.
Standing-wave ratio (VSWR)	S <sub>11,</sub> S <sub>22</sub> UII.//855 r, ♀ ↓ ●	50 Å ° 75 Å *	DIR. COUPL.
Return loss	s <sub>11, 522</sub> .ιοε. r, φ <b>j</b>	50 Å ° 75 Å *	DIR. COUPL.
Output reflection coefficient s22	s <sub>11, 522</sub> LIN. r, φ <b>Ι</b> ΟΓ Χ, Υ <b>Ι</b>	50 A ° 75 A *	DIR. COUPL.
Impedance	Z LIπ. τ, φ Ι • Or Χ,Υ Ι •	50 A ○ 75 A +	DIR. COUPL.
Normalized impedance		50 Å ° 75 Å *	DIR. COUPL.
Admittance			
	Υ LIN. r, φ I • Or X, Υ ] •	50 A ° 75 A *	DIR. Coupl.

### Group-delay measurement

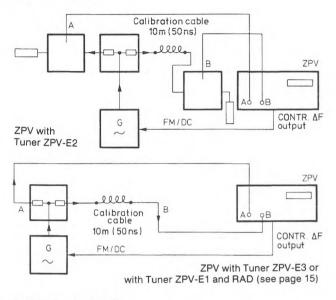
There are three main methods of measuring group-delay time. The choice of the best method for a given application is described in the Annex on page 38.

Independent of the method chosen, it is possible to store any value of group delay as a reference and to read off the variation in delay time relative to this value. This facility is described in more detail on page 25.

Calibration may or may not be required, depending on the method of measurement used.

### The FM-DC method

#### **Calibration setup**



#### **Calibration instructions**

Set required signal-generator frequency

Press A B or B/A
Press τ Cat.
Wait until 50 ±1 ns appears on the display

- Press AUTO
- According to the required frequency shift, press 40,4kitz o
  - SET fo +4kHz Or SET fo +40kHz

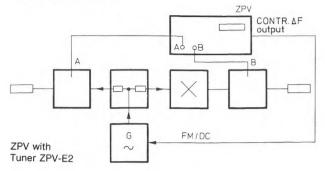
#### Notes on the calibration

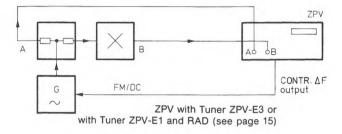
To obtain the highest possible accuracy, a calibration to

40 kHz deviation should be made using the key CAL

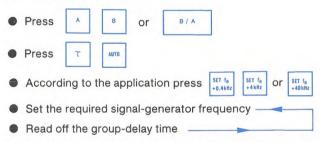
If other parameters, such as impedance or VSWR, have to be measured between group-delay measurements, it is not necessary to recalibrate, since the level at the output is stored in the ZPV.

#### Measurement setup





#### Measurement procedure

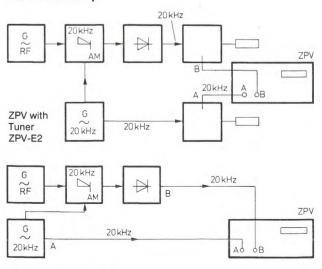


If the signal-generator frequency is slowly swept the group-delay time can be traced directly with a recorder.

The FM-DC method is particularly suited for rapid manual measurements. If a computer is used, only the static measurements should be used (next page).

#### The split-frequency method

#### **Calibration setup**

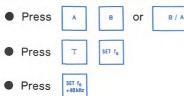


ZPV with Tuner ZPV-E3 or

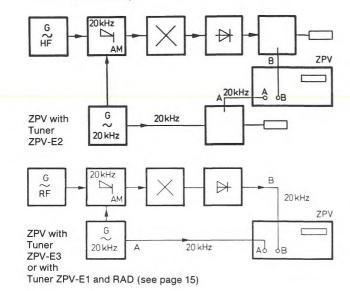
with Tuner ZPV-E1 and RAD (see page 15)

#### **Calibration instructions**

Set required signal-generator frequency



#### Measurement setup



#### **Measurement procedure**

- Press A
   B or
- Set required signal-generator frequency —
- Read result from display
- Group-delay time = 2 × displayed result (factor of 2 since modulation frequency is 20 kHz and not 40 kHz)

B / A

Note: After calibration the  $\tau$  key should not be

pressed again, since this would cause a false phase difference to be stored. Other parameters, such as  $s_{11}$ , can, however, be measured. To return to group-delay measurement it is only necessary to press one of the keys

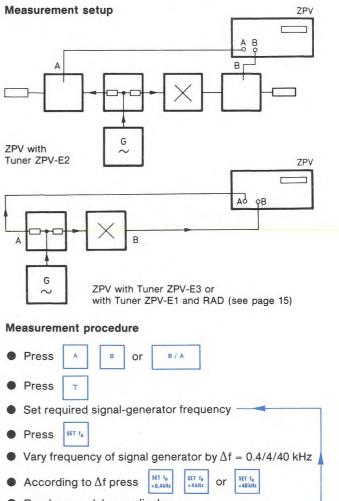
в B/A as shown above. or

The split-frequency method may be used for adjustments on all kinds of broadband test items since the ZPV always handles the 20-kHz signal and consequently does not have to resynchronize. The frequency limits of this measurement method are set by the modulator and demodulator and may lie outside the range of the ZPV.

With Tuner ZPV-E1 any split frequency may be used.

### Static (single) measurement of group delay

Calibration is not required with this method



Read group delay on display —

With Tuner ZPV-E1, any positive or negative deviation can be used, since this tuner has a built-in frequency counter. In this case in the next to the last step, instead of SET  $f_o$ 0.4, 4 or 40 kHz, the AUTO key should be pressed.

#### Storing a reference value

Regardless of the measurement method used it is possible in group-delay measurements, as in voltage measurements, to store any required reference value. This facility has many practical advantages, since it is often required to know the variations of the group-delay time rather than its absolute value.

#### Storage instructions

Adjust the group-delay time to be stored as reference

RECALL REF.

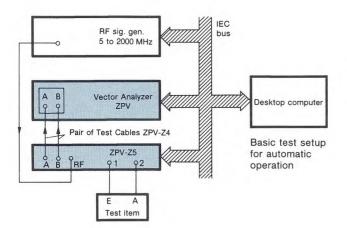
; the stored

- Store by pressing 9, 7 REF. STORE
- Check stored value by pressing value appears on the display
- Press AT

In the <u>ar</u> mode only the group-delay difference relative to the stored reference is displayed.

### System configuration, characteristics

When combining the Vector Analyzer ZPV with a programmable frequency generator and a controller, a **fully automatic network analyzer system** is obtained.



**Controller** In general, any desktop computer with an IECbus connection can be used as controller. Particularly suitable is the Process Controller PUC of Rohde & Schwarz. However, software for the Tektronix computers 4051 and 4052 and Hewlett Packard computers HP 9835 and HP 9845 can be supplied.

**Generator** Various Rohde & Schwarz generators are suitable for use with the ZPV, see table on page 8.

**Software** For this combination of instruments, Rohde & Schwarz offers easy-to-handle software so that a minimum of time is required to get acquainted with the application of the network analyzer. The preprogrammed measurement and display modes can be called up with code numbers. Graphic display in particular shows the efficiency of the basic software: the curves plotted can be made available directly as hardcopy documentation (for examples of programming and graphic display see page 28).

The resulting automatic network analyzer system is superior in many respects to the computer-controlled systems used hitherto: the high intelligence of the ZPV makes operation and programming simple and easy to understand. The test speed, in particular for impedance and admittance measurements, is very high since computing and control are performed to a large extent in the ZPV at optimum speed.

The **Basic Software** (ZPV-K1, -K4 or -K10 depending on type of computer) permits both easy programming of point-by-point measurements as they are required for final inspection and graphic display of continuous frequencydependent curves. There are different ways of outputting the test result: numerical display on the screen or by a printer and graphic display on the screen or output on a hardcopy unit. Comparing of nominal and actual values is also possible.

The **accuracy-improvement software** for use with the Network Analyzer permits fully automatic and extremely accurate s-parameter measurements over the entire frequency range of the tuner plug-ins.

The accuracy-improvement software includes the proven elements of the basic software plus an extension to enable corrected measurements. For this purpose, the test setup is measured prior to the test run using calibration standards. During the actual measurement the readings obtained from the ZPV are corrected in the desktop computer using the values specific to the test setup that were determined during calibration. The high-accuracy test result is displayed graphically or numerically on the screen of the computer.

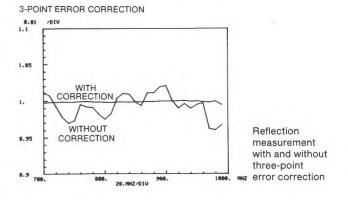
**Sources of error, requirements for correction** Basically measurements of the transmission factor and of the reflection coefficient have to be distinguished.

In **transmission measurements** errors are caused mainly by the frequency response of cables, test adapters and the instrument itself. All frequency-response errors can be eliminated by the so-called **simple error correction**.

**In reflection measurements** — using bridges or directional couplers — there are three main sources of error: a) directivity, b) mismatch at the test port, c) frequency response or frequency-dependent coupling attenuation between the test port and the test output. These errors are eliminated by so-called **three-point error correction** (using the accuracy-improvement software dispenses with the coupler in the reference channel).

Simple error correction can be used both for transmission measurements and reflection measurements with insertion heads or T junctions in the region of |r| = 0. It is based on the capability of the ZPV to perform measurements related to a reference value. For measurements over a wide frequency range, the reference values are stored in the desk-top computer.

**Three-point error correction** (see also page 39) is employed exclusively for reflection-coefficient measurements using bridges or directional couplers. In this case the ZPV readings are converted in the desktop computer after the correction factors have been established in the form of three complex constants by calibrated measurements (K<sub>1</sub> for the directivity of the test bridge, K<sub>2</sub> for the frequency response of the test setup and K<sub>3</sub> for the reflection coefficient of the bridge test port).



Since the s-parameter accuracy-improvement software is structured essentially the same as the basic software, the comments on the following pages apply also to the accuracy-improvement software. The code numbers for the basic- and accuracy-improvement software routines are given on page 43.

The following software, with detailed descriptions, is presently available from Rohde & Schwarz:

Process Controller PUC	ZPV-K10 291.8818.02
Tektronix 4051, 4052	ZPV-K1
HP 9835 and 9845	ZPV-K4 292.2413.02
-parameter accuracy-improvem	ent software for
-parameter accuracy-improvem Process Controller PUC	ent software for ZPV-K11 291.8918.02
-parameter accuracy-improvem Process Controller PUC Tektronix 4051, 4052	ent software for ZPV-K11 291.8918.02 ZPV-K2 292.2213.02

The following explanations and examples refer to the ZPV-K10.

### Basic software

#### Using the software

The basic software is written so that even those with no programming experience can use it easily. The very high level of operating ease has been achieved by compromising between speed, memory requirement, flexibility and simplicity. For most purposes the following simple commands will be adequate:

Y	Entry of a value, e. g. frequency in MHz
GOSUB XX	XX is a code number (see list on page 43) which defines the operation to be executed
END	End of the program

Example (see code number list)

Y = 4 GOSUB 1	The SMS2 is used as signal generator Basic setting of SMS2 (start of program)
Y = 20 GOSUB2	Frequency setting on SMS2: 20 MHz
GOSUB 50	Measurement of voltage in channel B, linear in mV by amplitude and phase

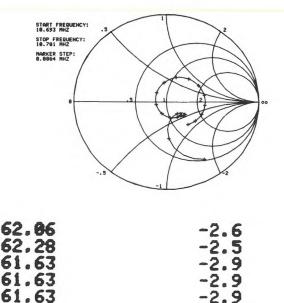
The basic software contains routines for frequency and level setting on the Rohde & Schwarz signal generators. These are called up by means of code numbers.

	SPN	SMS2	XPC SMPC SMPD	SWP	SMK
Address used	11	28	13	15	8
Basic setting using		Y = 4 GOSUB 1	Y = 5 GOSUB 1		Y = 7 GOSUB1
Level setting (e.g. 0 dBm)					
using	Y = 0 GOSUB3	Y = 0 GOSUB3	Y = 0 GOSUB3	Y = 0 GOSUB3	Y = 0 GOSUB3
Frequency se (e.g. 40 MHz)					
using		Y = 40 GOSUB2		Y = 40 GOSUB2	Y = 40 GOSUB2
Sweep routine	es				
Y = 40 GOSUB9	Sweep sta in MHz (e.			These ro are the s	
Y = 50 GOSUB 10	Sweep sto in MHz (e.		ncy	for all signal generators	
Y = 5	Sweep ste	p size			

#### **Documentation of measurement results**

For documentation of the results a printer or a hardcopy unit (for example, the Tektronix 4631) are recommended. The high-performance Universal Matrix Printers PUD 2 and PUD 3 (Order No's 359.5018.02 and 359.5501.02) are particularly suited for this. The PUD 2 is an impact printer with a printing speed of 80 characters/sec. The PUD 3 is an ink-jet printer with twice this speed – 150 characters/sec.

15120	Z(31)=0		
15130	Z(24)=0		
15140	Z(28)=0		
15150	Z(3) = 0		
15160	IF Z(27)<>0	THEN	15210



Examples of documentation: top: printer record of program section; centre and bottom: record produced on hardcopy unit (Smith diagram plot of results and table of values)

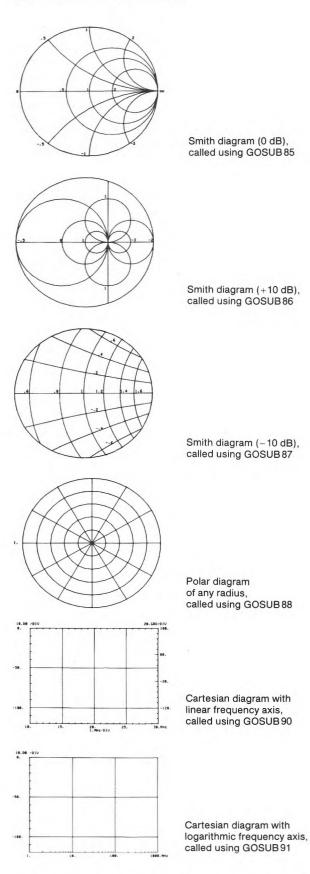
The ZPV is set ex works to the address 26.

in MHz (e.g. 0.5 MHz)

GOSUB11

### Summary of diagrams which can be called directly

(The scale is fixed automatically)



The diagrams are drawn very quickly, the Smith-circle diagram, for example, requires only about 4 seconds.

### Program preparation

#### General notes

As with other basic software packages supplied by Rohde & Schwarz the structure shown below has been used for the ZPV-K10:

lines 1 to 99 basic software lines 100 to 8999 free for user program lines 9000 to 32000 basic software

Thus the user has the lines 100 to 8999 and those following 32000 available for use. When programming with the basic software ZPV-K10 it must be remembered that the variables Q, W, X, Y, Z and combinations thereof may only be used in conjunction with the code number list in the user program.

Among the variables stored by the basic software are (for greater detail refer to manual of ZPV-K10):

- Z (1) = present frequency
- Z (2) = present level
- Z (7) = sweep start frequency
- Z(8) = sweep stop frequency using the sweep routines Z (9) = sweep step size
  - GOSUB 9, 10, 11.

These values are fixed

- Z (23) = choice of signal generator
- (3 = SPN, 4 = SMS2, 5 = XPC/SMPC/SMPD, 6 = SWP, 7 = SMK)
- Z (25) = multiplication factor for lefthand display
- Z (26) = multiplication factor for righthand display
- Z (30) = number of markers

Thus it can be seen that when, for example, a variety of different measurements is to be carried out it is not necessary to repeat the sweep routine in each case. The measured value is stored and read out via the variables X1 (lefthand display) and X2 (righthand display).

Note: The basic software automatically issues the command "TE" (external trigger - see page 31).

### Programming examples

In the following examples it will be assumed that the test setup, e.g. for impedance or group-delay measurement, has previously been calibrated manually. This is often the case in practice.

### Program start (principle)

- Basic setting of controller
- Basic setting of signal generator
- Level setting of signal generator

1st subprogram 2nd subprogram ..... nth subprogram

The program starts with the basic setting commands (do not forget the line numbers).

#### Example:

100 INIT	<ul> <li>basic setting of Tektronix 4051 calculator</li> </ul>
118 Y=4	(or 3, 5, 6, 7) basic setting on signal
120 GOSUB 1	generator, in this case the SMS2
138 Y=8	level setting, e.g. 0 dBm
140 GOSUB 3	
150 END	end of basic setting procedure

The program is started using RUN 100.

The actual program can now be written. Three possibilities are available:

#### 1. A single measurement

- Principle: 
   Frequency setting on signal generator
  - Execute required measurement
  - Output measured result —

Example 1:

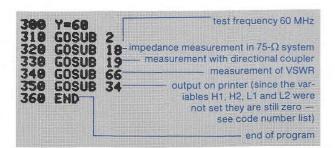
test frequency 10 MHz	30 Y=10	200
- measure B/A by amplitude and phase	IO GOSUB 2	210
output results on screen	30 GOSUB 33-	230
end of program	+0 ENU	240

The program is started using RUN 200.

10.00000	-3.90000	2.39200

Results displayed on screen

#### Example 2:



The program is started using RUN 300.

60.0000 2.03 Printout of result

#### 2. Sweep measurements without diagram

Principle:	Sweep routine
	Call required measurement ————————————————————————————————————
	Output result

Ε	x	а	m	pl	e	1
_	~	~	•••		-	2

409 Y=10 410 GOSUB 9 420 Y=20 430 GOSUB 10 440 Y=2	start frequency, here 10 MHz stop frequency, here 20 MHz step size 2 MHz	sweep routine
450 GOSUB 11 460 GOSUB 55- 470 GOSUB 35- 480 END	——— measurement of B//	and phase

#### The program is started using RUN 400.

10.00000	2.40300	-4.00000
12.00000	2.42500	-7.80000
14.00000	2.46989	-11.50000
16.00000	2.49700	-15.20000
18.00000	2.52509	-18.80000
29.00000	2.54700	-22.40000

Results displayed on screen

#### 3. Sweep measurements with diagram

Principle:	Sweep routine
	Select diagram
	Call required measurement
	Enter values in diagram — >

In sweep measurements with diagram display it is important that the GOSUB routines are executed in the correct

Step 4	+entry of result in diagram (GOSUB 96 to 98)
Step 3	+ single measurement (GOSUB 45 to 84)
Step 2	+diagram (GOSUB 85 to 92)
Step 1	sweep routine (GOSUB 9 to 11)
order:	

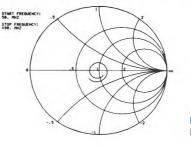
=complete measured curve on screen

The measured value (step 3) can only be entered (step 4) into the diagram when the diagram has been drawn. The sweep routine (step 1) must be executed before the diagram is called so that the marking of the scales, e.g. the frequency divisions on the cartesian plot, are known when the diagram is drawn. If a second curve is to be drawn on the same diagram (double scaling using GOSUB 89 and GOSUB 92) steps 2, 3 and 4 must be repeated.

#### Example:

588	Y=50 GOSUB	sweep routine with start frequency 50 MHz
520	Y=498	stop frequency 490 MHz
	GOSUB	19 step size 10 MHz
540	Y=10	
550	GOSUB	11
568	GOSUB	85 Smith diagram 0 dB
570	GOSUB	63-reflection factor in real and imaginary parts
580	GOSUB	96 presentation of results in diagram
590	END	end of program

The program is started using RUN 500.



Results shown in Smith diagram

### Special measurement problems

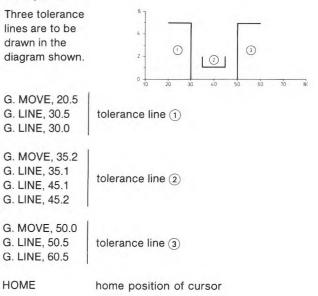
It is, of course, not possible to solve all measurement problems directly with the Basic Software ZPV-K10. The following paragraphs deal with some of the more commonly encountered cases.

Entering tolerance lines or special frequency markers in the diagram

The basic software is written so as to permit tolerance lines or special frequency markers to be entered without any additional conversion calculations. Three program instructions are enough:

G. MOVE, X <sub>1</sub> , Y <sub>1</sub>	the cursor jumps to the point defined by the coordinates $X_1  \text{and}  Y_1$		
G. LINE, X <sub>2</sub> , Y <sub>2</sub>	a line is drawn between the starting point $(X_1, Y_1)$ and the end point $(X_2, Y_2)$		
G. DRAW, X <sub>3</sub> , Y <sub>3</sub>	a point is marked at $X_3$ , $Y_3$		

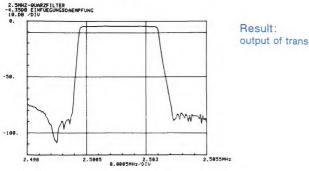
#### Example 1:



**Example 2:** A filter has a centre frequency of 2.50064 MHz. The transmission curve is to be drawn showing the two points at which the transmission loss has increased by 6 dB.

98 REN ** -6 DB BANDBREITE **	basic setting on signal generator, here XPC
28 GOSUB 1 38 Y=8	level setting on signal generator, here 0 dBm
40 GOSUB 3 50 Y=2.59064	setting to centre frequency (2.50064 MHz
50 GOSUB 2   70 GOSUB 58 80 A=X1	measurement of insertion loss at centre frequenc
90 Y=2.498 90 GOSUB 9 10 Y=2.5055 20 GOSUB 10 30 Y=5.0E-5	sweep routine wit start frequency 2.498 MH stop frequency 2.5055 MH step size 50 H
40 GOSUB 11 50 Y1=-120 60 Y2=0 70 S\$="DB" 80 T\$="2.5MHZ-QUARZF."	cartesian diagram with titl
20 GOSUB 50 30 GOSUB 97 40 MOVE Z(7),A-6	(NT(A\$100+.1)/100 – output insertion loss at centre frequence measurement of B/A (log.) – insertion los presentation of results in cartesian diagra cursor jumps to point with coordinates Z(7). A line drawn frem pairt Z(7). A to pairt Z(9). A
50 LINE 2(8);A~6 60 Home 70 End	line drawn from point Z(7), A-6 to point Z(8), A- cursor returns to home positio end of program

The program is started using RUN 100.



Result: output of transmission characteristic

# Programming without the Basic Software ZPV-K10

### General

In some applications it may be necessary to achieve exceptionally high measuring speeds. In such cases the basic software must be modified or a program must be written without using the basic software routines. The photograph on page 42 shows which characters must be used to address the individual keys of the ZPV. To help in remembering the abbreviated commands, mnemonic letter combinations were chosen. Thus for example:

CAL

CA (<u>C</u>HANNEL <u>A</u>): used to address the key

CL (<u>CAL</u>IBRATION): used to address the key

XY (XY COORDINATE SYSTEM): used to address the key XY I

The following characters are used frequently:

- SH (<u>SPEED HIGH</u>): increased measurement speed, only a single measurement is made without an average being formed, the recorder outputs are switched off
- SL (<u>SPEED LOW</u>): normal measuring rate, average value is formed by internal microprocessor of ZPV
- TE (<u>TRIGGER EXTERNAL</u>): the ZPV requires an external trigger pulse before a measurement is started, this can be provided by, e.g. LX, RX, LR, or with a secondary address such as 26.1, 26.2 or 26.3
- TI (<u>TRIGGER INTERNAL</u>): measurements are carried out continuously as in manual operation
- SR (<u>SEND REFERENCE</u>): reference values may be transferred to the controller as ASCII characters
- TR (<u>TAKE REFERENCE</u>): the values stored using SR are entered into the ZPV before making each measurement
- LR @ (Start measurement, Left and Right displays): the character @ is only accepted by the ZPV once the measurement is completed

The ZPV is set ex works to the address 26. Nine secondary addresses are also available.

### Using other signal generators

Special lines are available in the Basic Software ZPV-K10 for users wishing to measure with synthesizers other than those manufactured by Rohde & Schwarz (see examples below).

**Example 1:** A signal generator with programmable level and frequency setting is to be included in the basic software so that it can be called using Y = 8. The following changes will be required:

Basic setting on signal generator: 10 MHz, 0 dBm, modulation off

NEW	0150	IF Y $< > 8$ then 9155	
	9152		
NEW	9153	IEC OUT :	basic setting of signal generator
	12470	ON Z (23) GOSUB 12490, 12550, 12480, 12582,	5 5
		12480, 12382, 12586, 12485, 12487, 12590	
NEW	12590	IEC OUT :	level setting of signal generator
NEW	12591	RETURN	erginal generator
	12610	ON Z (23) GOSUB 12640, 12670, 12830, 12844, 12847, 12630, 12860, 12880	
NEW	12880	IEC OUT :	frequency setting of signal generator
NEW	12881	RETURN	

**Note:** The variable Z(23) in line 9100 is fixed according to the choice of signal generator.

## Example 2: Rapid measurement with ZPV and generator SPN

The ZPV outputs the measurement result in an ASCII string, which can be read into, for example, the string variable A\$ line 220 in program example below). To increase the measurement speed of the routine, the time-consuming conversion of the string "A\$ (old)" into a VAL function (line 210) can be performed in the following measurement cycle between the transmitter frequency setting/measurement start ZPV (line 190/200) and the measurement-value readout of the new string "A\$ (new)" (line 220). This overlapping assures that the transmitter and ZPV can synchronize or perform the measurement during the conversion.

Basic and level setting on SPN	Y=3:GOSUB1:Y=10:GOSUB3	100
Cartesian diagram	Z(7)=100:Z(8)=200:Z(9)=5	110
E " with title	Y1=-130:Y2=0:S\$="DB":T\$="AMPLITUDE"	120
Line 130: Measurement of B/A	G0SUB90:G0SUB58	130
amplitude and phase (GOSUB 58)	G.WIN,Z(7),Z(8),Y1,Y2	140
Specifying the first A\$	A\$="-120"	150
External triggering	IECOUT26, "TE"	160
Cursor in lower left corner of diagram	G.M,Z(7),-120 CL	170
Double loop to line 240	FORY=Z(7)TO Z(8) STEP Z(9)-	180
Frequency setting SPN	IECOUT11,STR\$(Y)+"KH"	190
Measurement start of ZPV	IECOUT, "LX"	200
Calculation of A\$ (old	X1=VAL (A\$)	210
Readout of ZPV indication in A\$ (new	IECIN26,A\$ Re	220
(old) for the previous frequency Y-Z (9	G.L, Y-Z (9), X1 Diagram input of X1 (old	230
	NEXTY	240
End of program	END-	250

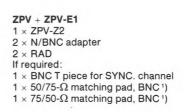
The section "MEASUREMENT AND CALIBRATION SET-UPS" indicated the basic setup needed for the various measurements. The tables which follow indicate in detail the components required for each setup. The full designation of the parts used is given in the table below:

Designation	Description	Order number
ZPV ZPV-E1 ZPV-E2 ZPV-E3	Vector Analyzer (basic unit) Tuner plug-in for basic unit (10 Hz to 50 MHz) Tuner plug-in for basic unit (0.1 to 1000 MHz) Tuner plug-in for basic unit (0.3 to 2000 MHz)	303.0510.02 292.0010.02
ZPV-K10 ZPV-K1 ZPV-K4	Basic software for Process Controller PUC Tektronix 4051, 4052 HP 9835, 9845	292.2113.02
ZPV-K11 ZPV-K2 ZPV-K5 ZPV-Z1 ZPV-Z2 ZPV-Z3 ZPV-Z4 ZPV-Z5 ZPV-Z6 ZWD-Z DNF SWOB4-Z ZRD2 RNA RNB RAD RMF	S-parameter accuracy-improvement software for Process Controller PUC Tektronix 4051, 4052 HP 9835, 9845 Insertion Adapter (at least two are required) Feed Unit Directional Coupler (50 $\Omega$ , 45 dB) Pair of Test Cables (N connectors) S-parameter Test Adapter DC Feed Unit Directional Coupler (75 $\Omega$ , 45 or 50 dB) Attenuator (10 dB, 50 $\Omega$ ) VSWR Bridge (10 to 1000 MHz, 50 $\Omega$ , 40 dB) VSWR Bridge (10 to 1000 MHz, 50 $\Omega$ , 40 dB) VSWR Bridge (10 to 1000 MHz, 50 $\Omega$ , 40 dB) VSWR Bridge (5 to 2500 MHz, 50 $\Omega$ , 46 dB) Precision Termination (50 $\Omega$ , N male) Termination (50 $\Omega$ , N male) Feed-through termination (only for Tuner ZPV-E1) Termination (50 $\Omega$ , N male) Short (50 $\Omega$ , N connectors) T piece (50 $\Omega$ , N connectors) T piece (50 $\Omega$ , N connectors) N/BNC adapter (50 $\Omega$ ) N/N coupling (50 $\Omega$ , male).	292.2213.02 292.2513.02 292.2713.50 292.2913.50 292.3110.50 335.1012.50 335.1112.52 265.3512.02 219.6270.70 272.4210.50 912.7003.00 912.7303.00 373.9017.52 272.4510.50 272.4910.50 272.50 272.50 272.50 272.50 272.50 275.50 275.50 275.5
	N/N coupling (50 $\Omega$ , female)	092.6700.00

Transmission measurements

Using Vector Analyzer ZPV with Tuner ZPV-E1 (10 Hz to 50 MHz)

**50** Ω 10 Hz to 50 MHz  $\begin{array}{l} \textbf{ZPV} + \textbf{ZPV-E1} \\ 1 \times \textbf{ZPV-Z2} \\ 2 \times \textbf{N/BNC} \ \text{adapter} \\ 2 \times \textbf{RAD} \\ \textbf{If required:} \\ 1 \times \textbf{BNC} \ \textbf{T} \ \textbf{piece for SYNC. channel} \end{array}$ 



X

75 Ω

10 Hz to 50 MHz

### Using Vector Analyzer ZPV with Tuner ZPV-E2 (0.1 to 1000 MHz)

**50** Ω 0.1 to 100 MHz

.

 $2 \times ZPV-Z1$   $1 \times ZPV-Z2$   $2 \times RNA (or RNB)$   $1 \times N/BNC adapter$  $1 \times N/N coupling (female)$ 

ZPV + ZPV-E2

**50** Ω 100 to 1000 MHz

**ZPV** + **ZPV-E2** as above plus: 2 × DNF  $\begin{array}{l} \textbf{ZPV} + \textbf{ZPV-E2} \\ 2 \times \text{ZPV-Z1} \\ 1 \times \text{ZPV-Z2} \\ 2 \times \text{RNA (or RNB)} \\ 1 \times \text{N/BNC adapter} \\ 1 \times \text{N/N coupling (female)} \\ 1 \times 50/75 \mbox{-} \Omega \mbox{ matching pad}^1) \\ 1 \times 75/50 \mbox{-} \Omega \mbox{ matching pad}^1) \end{array}$ 

**ZPV** + **ZPV-E2** as above plus: 1 × DNF 75 Ω

0.1 to 100 MHz

**75** Ω 100 to 1000 MHz

Using Vector Analyzer ZPV with Tuner ZPV-E3 (0.3 to 2000 MHz)

**50** Ω 0.3 to 2000 MHz **ZPV** + **ZPV-E3** 1 × ZPV-Z2

 $1 \times ZPV-Z4$  $1 \times N/BNC$  adapter

 $1 \times N/N$  coupling (female)

**ZPV** + **ZPV-E3** 1 × ZPV-Z2 1 × ZPV-Z4

 $1 \times N/BNC$  adapter

 $1 \times N/N$  coupling (female)

 $1 \times 50/75-\Omega$  matching pad<sup>1</sup>)

 $1 \times 75/50-\Omega$  matching pad<sup>1</sup>)

**75** Ω 0.3 to 2000 MHz

1) Not available from Rohde & Schwarz

**Reflection measurements** 



Using Vector Analyzer ZPV with Tuner ZPV-E2 (0.1 to 1000 MHz)

50 Q

0.1 to 100 MHz without directional couplers or VSWR bridge

ZPV + ZPV-E2 2 × ZPV-Z1 1 × ZPV-Z2 2 × RNA (or RNB) 1 × N/BNC adapter

not possible, since ZPV is 50  $\Omega$ 

50 Q

10 to 1000 MHz with Directional Couplers ZPV-Z3

ZPV + ZPV-E2 2 × ZPV-Z1 1 × ZPV-Z2 2 × ZPV-Z3  $3 \times \text{RNA} \text{ (or RNB)}$ 1 × N/BNC adapter 1  $\times$  short (50  $\Omega$ , N)  $2 \times \text{DNF}$ 

### ZPV + ZPV-E2 2 × ZPV-Z1

1 × ZPV-Z2  $2 \times ZWD-Z$ 

- $2 \times RNA (or RNB)$ 1 × N/BNC adapter
- 1 × short (Dezifix B)
- 4 × N/Dezifix A adapter
- $2 \times N/N$  coupling (female) 1 × 75- $\Omega$  termination<sup>1</sup>)

## 75 Q

**75**Ω

10 to 1000 MHz with Directional Couplers ZWD-Z

## **50** Ω

10 to 1000 MHz with **VSWR Bridge** SWOB4-Z

ZPV + ZPV-E2 2 × ZPV-Z1 1 × ZPV-Z2 1 × SWOB4-Z 3 × RNA (or RNB) 2 × DNF 1 × N/BNC adapter  $1 \times N/N$  coupling (female)  $1 \times N/N$  coupling (male)

- 1 × short (50  $\Omega$ , N)

ZPV + ZPV-E2

- $2 \times ZPV-Z1$  $1 \times ZPV-Z2$
- 1 × SWOB4-Z
- 2 × RNA (or RNB)
- $1 \times DNF$ 1 × N/BNC adapter
- $1 \times \text{short} (75 \Omega, N)$
- $1 \times 75 \Omega$  termination<sup>1</sup>)
- $1 \times N/N$  coupling (female, 75  $\Omega$ )<sup>1</sup>)
- $1 \times 50/75-\Omega$  matching pad<sup>1</sup>)
- $1 \times 75/50-\Omega$  matching pad<sup>1</sup>)

## **75** Ω

10 to 1000 MHz with **VSWR** Bridge SWOB4-Z

1) Not available from Rohde & Schwarz

**Reflection measurements** 

Using Vector Analyzer ZPV with Tuner ZPV-E1 (10 Hz to 50 MHz)

## 50 Q

- 10 Hz to 50 MHz T measurement without directional couplers or **VSWR** bridge
- ZPV + ZPV-E1 1 × ZPV-Z2
- 1 × RMF (50 Ω)
- 2 × N/BNC adapter
- 1 × BNC angle piece1)
- 1 × BNC T piece
- $2 \times RAD$
- 1 × matched measurement cable pair of same length, BNC, 50 Ω1)
- If required:
- 1 × BNC T piece for SYNC. channel
- ZPV + ZPV-E1 1 × ZPV-Z2
- $1 \times \text{RMF} (75 \Omega)$
- 2 × N/BNC adapter
- 1 × BNC angle piece<sup>1</sup>)
- $1 \times BNC T piece$
- $2 \times RAD$

If required:

- 1  $\times$  matched measurement cable pair of same length, BNC, 75  $\Omega^{\,1})$

1 × BNC T piece for SYNC. channel

- $1 \times 50/75-\Omega$  matching pad, BNC <sup>1</sup>) 1  $\times$  75/50- $\Omega$  matching pad, BNC <sup>1</sup>)
- 75 Q
- 10 Hz to 50 MHz T measurement
- without directional couplers or **VSWR** bridge

### Using Vector Analyzer ZPV with Tuner ZPV-E3 (0.3 to 2000 MHz)

## **50** Ω

0.3 to 2000 MHz T measurement without directional couplers or **VSWR** bridge

#### 1 × ZPV-Z2 1 × ZPV-Z4 1 × RNA (or RNB) $1 \times N$ angle piece 1 × N T piece 1 × N/BNC adapter

ZPV + ZPV-E3

- ZPV + ZPV-E3 1 × 7PV-72
  - 1 × ZPV-Z4
  - $1 \times 75-\Omega$  termination<sup>1</sup>)
  - $1 \times N T$  piece (75  $\Omega$ )<sup>1</sup>)
  - 1 × N/BNC adapter
- $1 \times 50/75-\Omega$  matching pad<sup>1</sup>)  $1 \times 75/50-\Omega$  matching pad<sup>1</sup>)
- T measurement without directional couplers or

75 Q

0.3 to 2000 MHz

**VSWR** bridge

**50** Ω

10 to 1000 MHz with Directional Coupler ZPV-Z3

## 50 Q

5 to 2000 MHz with **VSWR Bridge** ZRB

ZPV + ZPV-E3  $1 \times ZPV-Z2$ 1 × ZPV-Z4  $2 \times ZPV-Z3$ 1 × RNA (or RNB)  $1 \times \text{short} (50 \Omega, N)$ 1 × N/BNC adapter

ZPV + ZPV-E3

1 × RNA (or RNB)

 $1 \times \text{short} (50 \Omega, N)$ 

1 × N/BNC adapter

1 × N/N coupling (male)

1 × ZPV-Z2

1 × ZPV-Z4

 $1 \times ZRB$ 

ZPV + ZPV-E3  $1 \times ZPV-Z2$ 1 × ZPV-Z4  $2 \times ZWD-Z$ 1 × N/BNC adapter 1 × short (Dezifix B)  $1 \times 75-\Omega$  termination

# 4 × N male/Dezifix A adapter 2 × N/N coupling (female)

**75**Ω 10 to 1000 MHz with Directional Coupler ZWD-Z

**75**Ω

10 to 1000 MHz with **VSWR** Bridge SWOB4-Z

1 × ZPV-Z4 1 × SWOB4-Z  $1 \times \text{short} (75 \Omega, N)$ 1 × N/BNC adapter  $1 \times 75 \cdot \Omega$  termination<sup>1</sup>)  $1 \times N/N$  coupling (female, 75  $\Omega$ )<sup>1</sup>)  $1 \times 50/75-\Omega$  matching pad<sup>1</sup>)  $1 \times 75/50-\Omega$  matching pad<sup>1</sup>)

ZPV + ZPV-E3

1 × ZPV-Z2

### 1) Not available from Rohde & Schwarz

### 35

Reflection and transmission measurements

Using Vector Analyzer ZPV with Tuner ZPV-E2 (0.1 to 1000 MHz)

50 Ω

0.1 to 100 MHz without directional couplers or VSWR bridge  $\begin{array}{l} \textbf{ZPV + ZPV-E2} \\ 3 \times ZPV-Z1 \\ 1 \times ZPV-Z2 \\ 2 \times RNA (or RNB) \\ 1 \times N/BNC \ adapter \\ 1 \times N/N \ coupling \ (female) \end{array}$ 

not possible, since ZPV is 50  $\Omega$ 

## **50** Ω

**10 to 1000 MHz** with Directional Couplers ZPV-Z3  $\begin{array}{l} \textbf{ZPV} + \textbf{ZPV-E2} \\ 3 \times \text{ZPV-Z1} \\ 1 \times \text{ZPV-Z2} \\ 3 \times \text{ZPV-Z3} \\ 4 \times \text{RNA (or RNB)} \\ 1 \times \text{N/BNC adapter} \\ 1 \times \text{short (50 } \Omega, \text{N)} \\ 1 \times \text{N/N coupling (female)} \\ 1 \times \text{N/N coupling (male)} \end{array}$ 

**ZPV + ZPV-E2**   $3 \times ZPV-Z1$   $1 \times ZPV-Z2$   $3 \times ZWD-Z$   $4 \times RNA (or RNB)$   $1 \times N/BNC adapter$   $1 \times short (Dezifix B)$   $4 \times N/N coupling (female)$  $6 \times N male/Dezifix A adapter$ 

**75** Ω 10 to 1000 MHz

**75**Ω

with Directional Couplers ZWD-Z

**75**Ω

10 to 1000 MHz

with

**VSWR Bridge** 

SWOB4-Z

## 50 Ω

10 to 1000 MHz with VSWR Bridge SWOB4-Z  $\begin{array}{l} \textbf{ZPV} + \textbf{ZPV-E2} \\ 3 \times \textbf{ZPV-Z1} \\ 1 \times \textbf{ZPV-Z2} \\ 1 \times \textbf{SWOB4-Z} \\ 3 \times \textbf{RNA} (or \textbf{RNB}) \\ 2 \times \textbf{DNF} \\ 1 \times \textbf{N/BNC} adapter \\ 1 \times \textbf{N/N} coupling (female) \\ 1 \times \textbf{N/N} coupling (male) \end{array}$ 

**ZPV** + **ZPV-E2** 3 × ZPV-Z1

- $1 \times ZPV-Z2$
- 1 × SWOB4-Z
- $3 \times RNA$  (or RNB)  $1 \times DNF$
- $1 \times \text{DNF}$ 1 × short (75  $\Omega$ , N)
- 1 × N/BNC adapter
- $1 \times N/N$  coupling (female, 75  $\Omega$ )<sup>1</sup>)
- $1 \times 50/75-\Omega$  matching pad<sup>1</sup>)
- $2 \times 75/50-\Omega$  matching pad<sup>1</sup>)

1) Not available from Rohde & Schwarz

### Reflection and transmission measurements



Using Vector Analyzer ZPV with Tuner ZPV-E1 (10 Hz to 50 MHz)

**50** Ω

**10 Hz to 50 MHz** T measurement or with directional coupler or with VSWR bridge See listings for "Transmission measurements" and "Reflection measurements" (N/BNC adapters and 2 × RAD also required — see page 15) See listings for "Transmission measurements" and "Reflection measurements" (N/BNC adapters and 2 × RAD also required — see page 15)

10 Hz to 50 MHz T measurement or with directional coupler or with VSWR bridge

**75** Ω

## 50 Ω

### Using Vector Analyzer ZPV with Tuner ZPV-E3 (0.3 to 2000 MHz)

## 0.3 to 2000 MHz

T measurement without directional couplers or VSWR bridge See listings for "Transmission measurements" and "Reflection measurements" See listings for "Transmission measurements" and "Reflection measurements"

## **75** Ω

0.3 to 2000 MHz T measurement without directional couplers or VSWR bridge

## 50 Ω

**10 to 1000 MHz** with Directional Couplers ZPV-Z3

## 50 Ω

5 to 2000 MHz with VSWR Bridge ZRB  $\begin{array}{l} \textbf{ZPV} + \textbf{ZPV-E3} \\ 1 \times \textbf{ZPV-Z2} \\ 1 \times \textbf{ZPV-Z4} \\ 2 \times \textbf{RNA} (or \textbf{RNB}) \\ 3 \times \textbf{ZPV-Z3} \\ 1 \times \textbf{short} (50 \ \Omega, \textbf{N}) \\ 1 \times \textbf{N/BNC} adapter \end{array}$ 

- 1 × N/N coupling (female)
- 1 × N/N coupling (male)

**ZPV** + **ZPV-E3** 1 × ZPV-Z2 1 × ZRB 1 × RNA (or RNB) 1 × short (50 Ω, N) 1 × ZPV-Z4 1 × N/NC adapter 1 × N/N coupling (male)  $\begin{array}{l} \textbf{ZPV} + \textbf{ZPV-E3} \\ 1 \times \text{ZPV-Z2} \\ 1 \times \text{ZPV-Z4} \\ 2 \times \text{RNA (or RNB)} \\ 3 \times \text{ZWD-Z} \\ 1 \times \text{short (Dezifix B)} \\ 1 \times \text{N/BNC adapter} \\ 6 \times \text{N male/Dezifix A adapter} \\ 4 \times \text{N/N coupling (female)} \end{array}$ 

**75** Ω 10 to 1000 MHz

> with Directional Couplers ZWD-Z

 $\begin{array}{l} \textbf{ZPV} + \textbf{ZPV-E3} \\ 1 \times \textbf{ZPV-Z2} \\ 1 \times \text{RNA (or RNB)} \\ 1 \times \text{short } (75 \ \Omega, \ N) \\ 1 \times \text{SWOB4-Z} \\ 1 \times \text{N/BNC adapter} \\ 1 \times \textbf{ZPV-Z4} \\ 1 \times \text{N/N coupling (female, 75 \ \Omega)^1)} \\ 1 \times 50/75-\Omega \ \text{matching pad^1)} \\ 2 \times 75/50-\Omega \ \text{matching pad^1)} \end{array}$ 

## **75** Ω

10 to 1000 MHz with VSWR Bridge SWOB4-Z

1) Not available from Rohde & Schwarz

## ANNEX

### Group-delay measurement

A two-port network can vary the signal applied at its input in two ways:

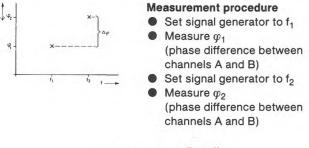
in the amplitude and

in the phase.

**Amplitude distortions** can be detected by means of a transmission measurement (see example 6 on page 12). Group-delay measurement on the other hand is concerned with the nonlinear **phase distortions** introduced by the transmission network. The group-delay time is defined as:

$$\tau = \frac{\mathrm{d}\,\varphi}{\mathrm{d}\,\omega} = \frac{\mathrm{d}\,\varphi}{2\,\pi\,\mathrm{df}}$$

In general, the phase difference  $\Delta \varphi$  occurring between two frequencies f<sub>1</sub> and f<sub>2</sub> is measured and referred to the frequency difference (see diagram below).



**Result:** 
$$\tau = \frac{\varphi_2 - \varphi_1}{360^\circ \cdot (f_2 - f_1)}$$

The smaller the frequency difference is chosen, the smaller is, as a rule, the measured phase difference  $\Delta \varphi$ . This calls for an extremely accurate phase meter. If the frequency difference is chosen too large, false results may be obtained when measuring narrowband test items.

#### A good rule-of-thumb is:

To measure the group-delay time with an accuracy of 1 ns using a frequency change of  $\Delta f = 27$  kHz, the phase meter must have a resolution of one hundredth of a degree. This can be seen from the formula:

$$\tau = \frac{\Delta \varphi}{360^{\circ} \cdot \Delta f} = \frac{1/_{100}}{360 \cdot 27 \cdot 10^3} = 10^{-9} \, [s].$$

The difficulty in the measurement of group-delay time is to obtain a **direct** readout of the result. Previous solutions involved the use of a scale calibrated for one particular frequency change  $\Delta f$ . Measurements with other values of  $\Delta f$  involved complicated conversion. This time-consuming procedure has been reduced to a minimum thanks to the microprocessor used in the ZPV.

Three main methods of measuring group-delay time are available.

### The FM-DC method

A signal generator with FM-DC modulation capability is varied in frequency by the required value  $\Delta f$  (40 kHz, 4 kHz, 400 Hz). Before an actual measurement can be made the setup must be calibrated.

With this setup, the voltage step at the DC output of the ZPV, which drives the FM-DC input of the signal generator, is increased until the frequency change is sufficient to produce a reading of exactly 50 ns on the ZPV. This completes the calibration procedure. When the test item is now connected in place of the calibration cable the values of  $\tau$  can be measured **directly** in microseconds.

The calibration cable with a group-delay time of 50 ns is supplied with the ZPV.

#### The split-frequency method

In the split-frequency method (test setup, page 25) the RF signal from the signal generator is frequency or amplitude modulated, usually at 20 kHz, and demodulated again at the output of the test item. The phase difference between the 20-kHz reference signal and the 20-kHz signal recovered by demodulation is used to calculate the group-delay time.

This procedure is applicable with Tuners ZPV-E2 and E3, since their sampling stages convert the input signal to an intermediate frequency of 20 kHz. In the split-frequency method even broadband sweeping is possible, since the ZPV only receives the 20-kHz signal at all times. There is no resynchronization. The frequency limits of the sweep are determined only by the modulator and demodulator, and may even lie outside the range of the ZPV.

When the Tuner ZPV-E1 is employed, any desired split-frequency can be used. This is particularly important in the case of narrowband test items.

#### Drawbacks of this methód

Additional equipment required (modulator and demodulator), additional errors due to delay time of modulator and demodulator. The errors can be eliminated by using a symmetrical setup with a second demodulator in channel A.

#### Advantage

Broadband sweep operation, **even outside** the range of the ZPV.

The static (single) measurement of group-delay

The signal generator is shifted in frequency by a certain amount, either manually or under computer control. For manual measurements:

 $f_2 = f_1 + 400 \text{ Hz} \text{ (or } 4 \text{ kHz or } 40 \text{ kHz} \text{)}.$ 

Since additional calculations are no problem when using a computer, any frequency shift can be employed in this case.

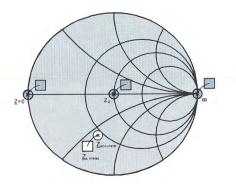
According to the chosen frequency step, the ZPV can be used to measure group-delay with the following resolution:

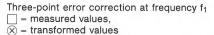
 $\Delta f = 40 \text{ kHz}$ : resolution 1 ns  $\Delta f = 4 \text{ kHz}$ : resolution 10 ns  $\Delta f = 400 \text{ Hz}$ : resolution 100 ns

The built-in frequency counter of the Tuner ZPV-E1 permits the use of any desired frequency deviation (see also page 25).

### Three-point error correction

Three-point error correction is employed to eliminate errors caused by the test setup as far as possible. According to this method the **short circuit** ( $\mathbf{Z} = \mathbf{0}$ ), matching ( $\mathbf{Z}_0$ ) and **open circuit** ( $\infty$ ) are measured at a certain frequency f<sub>1</sub> by the network analyzer (see following diagram) and are transformed in an external computer into the ideal values plotted on the horizontal axis of the Smith chart. When connecting now an unknown test item to the test setup and transforming the measured value ( $Z_{x meas}$ ) as before, the accurate impedance value ( $Z_{accurate}$ ) of the test item is obtained.



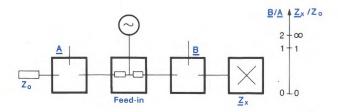


The error in measurement is only about 1% referred to the reflection coefficient even on the outer circle of the Smith chart. Additional errors caused by inaccurate frequency setting of the generator can be largely avoided by using a synthesizer. For more than one test frequency calibration routines must be available for each further frequency.

# Impedance measurements on high-impedance circuit elements

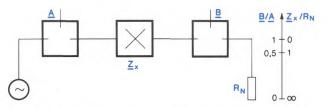
However, even with the use of 3-point correction, the network analyzer cannot distinguish between impedance values above 10 k $\Omega$ , because of a residual error of about 1% on the outer circle.

The following block diagram shows the simplest type of reflection measurement not using a VSWR bridge or a directional coupler. As can be seen from the nomogram, a small error in the measured voltage ratio  $\underline{B}/\underline{A}$  results at a high impedance ( $\gg Z_0$ ) in a large error in  $\underline{Z}_x$ . This method is thus unsuited for high impedances for all network analyzers at present on the market.



Dependence of measurement result derived from  $\underline{B}/\underline{A}$  value on the impedance  $\underline{Z}_x$  (in a reflection measurement)

If the network analyzer also has the capability of operating according to the voltage-divider principle (see following block diagram) and to convert the measured values into impedances, it will be able to measure values in the M $\Omega$  range at frequencies up to 100 MHz.



Dependance of measurement result derived from <u>B/A</u> value on the impedance  $\underline{Z}_x$  (using voltage-divider principle)

In this type of operation, the unknown 2-pole  $Z_x$  forms a voltage divider with a standard resistance  $R_N$ . A 50- $\Omega$  resistance is used, but other resistance values would also be satisfactory. It is possible to measure by this method with the ZPV. The microprocessor of the ZPV, after its HIGH Z key is pressed, computes the unknown impedance from the voltage ratio B/A according to the formula

$$Z_{x} = \left(\frac{\underline{V}_{A}}{\underline{V}_{B}} - 1\right) \cdot \mathbf{R}_{N}$$

**Calibration:** To eliminate the effect of variation in the ZPV frequency response, the ZPV can be calibrated at every measurement frequency by replacing the test item by a short circuit and pressing the PARAM. CAL. key. The measurement of the voltage ratio  $\underline{B/A}$  is then made in the operating mode  $\underline{B/A}$ , LIN./REF. (for more details see "News from Rohde & Schwarz", Vol. 87).

# Principal parameters of directional couplers and VSWR bridges

Since directional couplers and VSWR bridges only achieve perfect separation of the incident and reflected waves in theory, parameters have been introduced to describe their performance in practice (see measurement example 7 on

page 13). The **transmission or insertion loss** is a frequency dependent quantity which indicates the extent to which the applied RF power is attenuated before reaching the measuring

The **coupling attenuation** indicates the extent to which the power reflected from the test item is attenuated before reaching the measuring port. This parameter is strongly frequency dependent and determines the lowest usable frequency of the directional coupler or VSWR bridge.

The **directivity** expresses the ratio of the reflected wave to the unwanted component of the incident wave appearing at the measurement port. The greater the directivity, the lower the error introduced by the directional coupler or VSWR bridge (typical value 45 dB).

The lower the **standing-wave ratio** or intrinsic coefficient of the directional coupler or VSWR bridge, the more accurate will be the measurement. The relation between the two

is: VSWR =  $\frac{1+r}{1-r}$ .

port.

## ANNEX

### Frequently used formulas

$$\begin{array}{ll} \mbox{Impedance} & \underline{Z} = Z_0 \cdot \frac{1+r}{1-r} = \mathsf{R} + \mathsf{j} \mathsf{X} = Z \cdot e^{\mathsf{j} \phi_Z} \\ \mbox{Special cases: short} & (Z=0): r=-1 \\ & \text{open} & (Z=\infty): r=+1 \\ & \text{match termination} & (Z=Z_0): r=0 \end{array} \\ \mbox{Admittance} & \underline{Y} = \frac{1}{\underline{Z}} \\ \mbox{Standing-wave ratio (VSWR)} & VSWR = \frac{V_{max}}{V_{min}} = \frac{1+r}{1-r} \\ \mbox{Reflection coefficient} & \underline{r} = r \cdot e^{\mathsf{j} \phi_T} = \mathsf{r}_x + \mathsf{j} \mathsf{r}_y = \frac{\mathsf{b}_1}{\mathsf{a}_1} = \mathsf{s}_{11} \text{ (see s parameters)} \\ \mbox{Return loss} & = 20 \ \text{lgr} \\ \mbox{Transmission loss} & = 20 \ \text{lg} \frac{\mathsf{b}_2}{\mathsf{a}_1} \text{ (see s parameters)} \\ \mbox{Attenuation (or gain)} & = 20 \ \text{lg} \frac{\mathsf{b}_2}{\mathsf{a}_1} \text{ (see s parameters)} \end{array}$$

Relationship between reflection coefficient  $\underline{r}$  and measured quotient  $\underline{B}/\underline{A}$ 

a) without directional couplers or VSWR bridge  $\frac{\underline{B}}{\underline{A}} = 1 + \underline{r}$ 

b) with directional couplers or VSWR bridge  $\frac{\underline{B}}{\underline{A}} = \underline{r}$ 

Group-delay time 
$$\tau = \frac{\Delta \varphi}{2 \pi \Delta f}$$

S parameters



Definitions: Waves entering the twoport: a<sub>1</sub>, a<sub>2</sub> Waves leaving the twoport: b<sub>1</sub>, b<sub>2</sub> (blue)

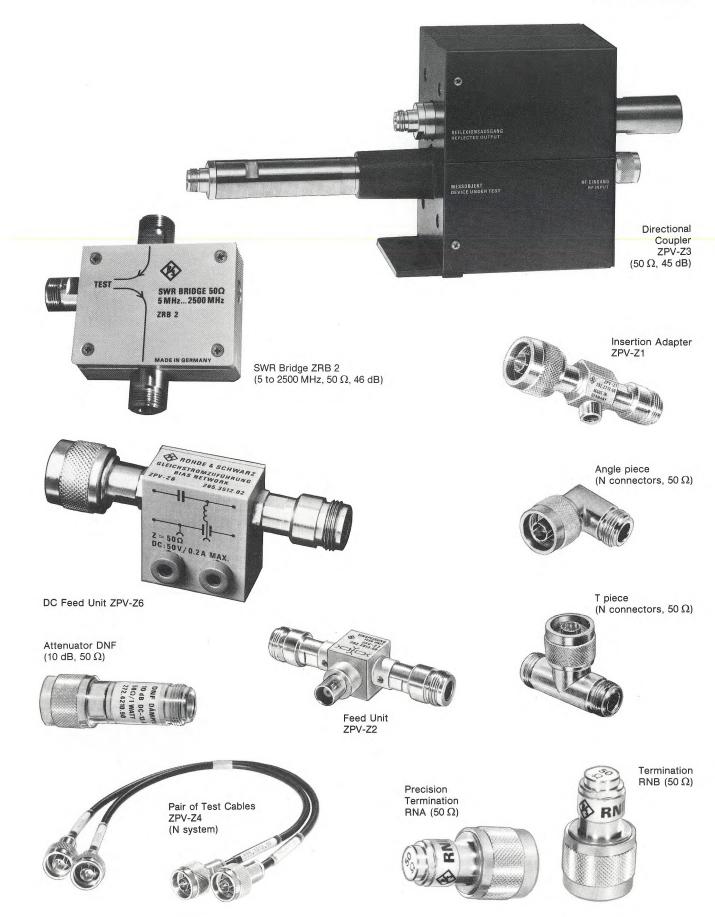
Input reflection coefficient  $s_{11} = \frac{b_1}{a_1} | a_2 = 0$ Output reflection coefficient  $s_{22} = \frac{b_2}{a_2} | a_1 = 0$ Forward transmission coefficient  $s_{21} = \frac{b_2}{a_1} | a_2 = 0$ 

Reverse transmission coefficient  $s_{12} = \frac{b_1}{a_2} \begin{vmatrix} a_1 = 0 \end{vmatrix}$ 



### Important extras for ZPV

(to different scales)



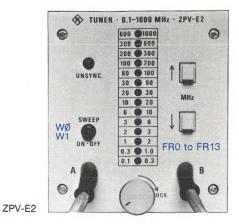
## PROGRAMMING

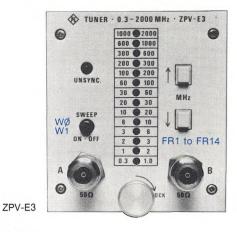
Setting com	mands (see also photos on right)
Control character (the trailing dots stand for the numer to be inserted)	Setting rics
AR B0/B1 FR G0/G1 H0/H1 HZ K0/K1 N0N3 PO RZ SH SL SL TE TI TE TI TR TS	amplitude range button B, U $\times$ 10 OFF/ON (ZPV-E1) frequency range tendency indication OFF/ON button A, U $\times$ 10 OFF/ON (ZPV-E1) frequency value recorder output OFF/ON filter setting (ZPV-E1) phase offset reference value (HIGH-Z measurement) high measurement speed normal measurement speed external triggering internal triggering reference value (10 ASCII characters) device status word (10 ASCII characters)

### Output commands

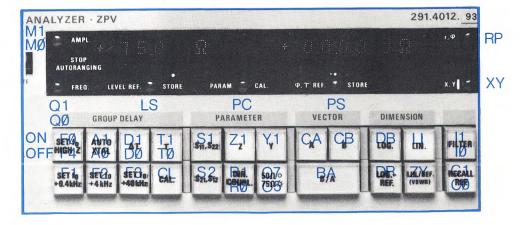
Contro		dary address	Output
charac			
	ASCII	PUC/	
1.1.4	code	Tek 4051/4052	
LX	a	1	lefthand readout
RX	b	2	righthand readout
LR	С	3	lefthand and right-
			hand readouts
DS	d	4	device status word
			(coded)
BA	е	5	measurement range
			of channel A
BB	f	6	measurement range
1.0		•	of channel B
BE	q	7	frequency range of
TH .	y	1	plug-in
AD	h	8	DC voltage of ADC
AU	11	0	
0.0		0	female connector
SR	i	9	reference value
FV	j	10	frequency at SYNC
			input
			(with Tuner ZPV-E1
			only)







Association of programming commands (blue) with ZPV operating controls



## CODE NUMBER LIST

Code number list of Basic Software and S-parameter Accuracy-improvement Software for Process Controllers PUC from Rohde & Schwarz, Tektronix 4051 and 4052 and

Hewlett Packard 9835 and 9845 (no graphics).

Y = 3 ger	erator SMLU Y = 5 generator XPC erator SPN SMPC/SMPD erator SMS2 Y = 6 generator SW Y = 7 generator SM
Input data         2 test frequency         3 test level         6 shift of reference plane         7 relative dielectric constant ε,         9 sweep start frequency         10 sweep stop frequency         11 sweep stop trequency         13 number of markers         (not with HP 9835 and 9845)         14 frequency deviation for group         measurement	-delay Physical unit MHz MHz MHz KHz (Basic Software only)
Operational settings           17 impedance of test setup 75.07           18 impedance of test setup 75.07           19 parameter measurement usin couplers           21 parameter measurement with couplers           19 measurement with insertion u           11 measurement with directional coupler or VSWR bridge           17 measurement with T junction           22 filter on           23 filter off           25 electrical length compensatio           26 electrical length compensatio	g directional out directional nit S-parameter Accuracy- improvement Software
Program execution 39 queuing 1 s 41 queuing 0.1 s	42 program stop 43 print out
Charts (not with HP 9835 and 98- 85 Smith chart 86 Smith chart +10 dB 87 Smith chart -10 dB 88 polar diagram 99 additional scaling, polar 90 cartesian diagram, linear frequency axis 91 cartesian diagram, log frequency axis 92 additional scaling, cartesian	<ul> <li>45)</li> <li>T\$ - "(title, max. 20 characters)"</li> <li>T\$ - "(title, max. 20 characters)"</li> <li>T\$ - (title, max. 20 characters)"</li> <li>Y - outer circle</li> <li>T\$ - "(title, max. 20 characters)"</li> <li>Y - outer circle</li> <li>Y1 - minimum vertical axis</li> <li>Y2 - maximum vertical axis</li> <li>S\$ - "(unit, max. 3 characters)"</li> <li>T\$ - "(title, max. 20 characters)"</li> <li>input same as under 90</li> </ul>

- 97 magnitude (real component) in cartesian coordinates 98 phase (imaginary component, group delay) 99 in cartesian coordinates

Basic software	
30 calibrate parameter	alues al component) as reference value ary component), group delay as reference value c group-delay measurement
Output of single-shot r 33 output on display 34 output on printer	neasurements         H1 = upper limit of magnitude (real component)         H2 = upper limit of phase (imaginary component)         L1 = lower limit of magnitude (real component)         L2 = lower limit of phase (imaginary component)
Output of swept-freque 35 output on display 37 output on printer	ncy measurements limit input same as under 33 and 34

	voltage measurement	linear	Physical unit mV, degrees
	channel A	in loui	my, degrees
46	voltage measurement	linear, relative	no dimensior
	channel A	and a second	degrees
47	voltage measurement	log	dBm, degree
	channel A	log	abili, degree
49	voltage measurement	log, relative	dB, degrees
	channel A	iog, relative	ub, degrees
50	voltage measurement	linear	mV, degrees
	channel B	inical	mv, degrees
51	voltage measurement	linear, relative	no dimensior
<u>.</u>	channel B	inical, relative	degrees
53	voltage measurement	log	
	channel B	log	dBm, degree
54	voltage measurement	log, relative	
•	channel B	log, relative	dB, degrees
55	voltage ratio measure-	linear	no dimonsiar
	ment, channel B/A	inidal	no dimensior
57	voltage ratio measure-	linear, relative	degrees
01	ment, channel B/A	initeal, relative	no dimensior
58	voltage ratio measure-	log	degrees
00	ment, channel B/A	iog	dB, degrees
59	voltage ratio measure-	log, relative	
00	ment, channel B/A	iog, relative	dB, degrees
66 67	measurement reflection coefficient measurement VSWR measurement impedance measurement impedance measurement	and imaginary components log by magnitude and phase by magnitude and phase in terms of resistance	no dimension dB, degrees no dimension degrees Ω, degrees Ω
	and reactance		
13	admittance measurement	by magnitude and phase	mS, degrees
14	admittance measurement	In terms of conductance	mS
75	and susceptance	19-1	
13	transmission factor	linear by magnitude	no dimensior
77	measurement transmission factor	and phase	degrees
11	transmission factor	linear with real	no dimension
	measurement	and imaginary	
70	transmission faster	components	
10	transmission factor	log by magnitude	dB, degrees
	measurement	and phase	
Gro	oup-delay measurement		
82	static group-delay measur	ement	μs
-	voltage measurement		
DC	voltage measurement		

S-parameter Accuracy-improvement	Software
Measurements 45 s <sub>11</sub> or s <sub>22</sub> measurement without correction	Physical unit no dimension,
46 s <sub>11</sub> or s <sub>22</sub> measurement with correction	degrees no dimension,
47 $s_{11}$ or $s_{22}$ measurement with 3-point correction	degrees no dimension, degrees
49 s <sub>21</sub> or s <sub>12</sub> measurement without correction	no dimension, degrees
50 $s_{21}$ or $s_{12}$ measurement without correction 51 $s_{21}$ or $s_{12}$ measurement with correction	dB, degrees no dimension,
53 s <sub>21</sub> or s <sub>12</sub> measurement with correction	degrees dB, degrees
54 B/A measurement without correction	no dimension, degrees
55 B/A measurement without correction 57 B/A measurement with simple correction	dB, degrees no dimension,
58 B/A measurement with simple correction	degrees dB, degrees
59 Z-measurement without correction 61 Z-measurement with simple correction 62 Z-measurement with 3-point correction	Ω, jΩ Ω, jΩ Ω, jΩ
Measurement using S-parameter Test Adapter ZPV-	Z5
$ \begin{array}{cccc} 70 & s_{11} \text{ measurement} & 73 & s_{21} \text{ measure} \\ 71 & s_{22} \text{ measurement} & 74 & s_{12} \text{ measure} \\ \end{array} $	ement
Calibration 33 calibration for simple correction 35 calibration for 3-point correction 63 calibration for simple correction 65 calibration for 3-point correction only for logarit	hmic diagram
Numerical output of measurements 37 output on display 38 output on printer	



GmbH & Co. KG · D-8000 München 80 · Mühldorfstr. 15 · Tel. (089) 4129-0 Int. +49894129-0 · Telex 523703 Printed in the Fed. Rep. of Germany · Subject to change · Data without tolerances: order of magnitude only 285 (F)